

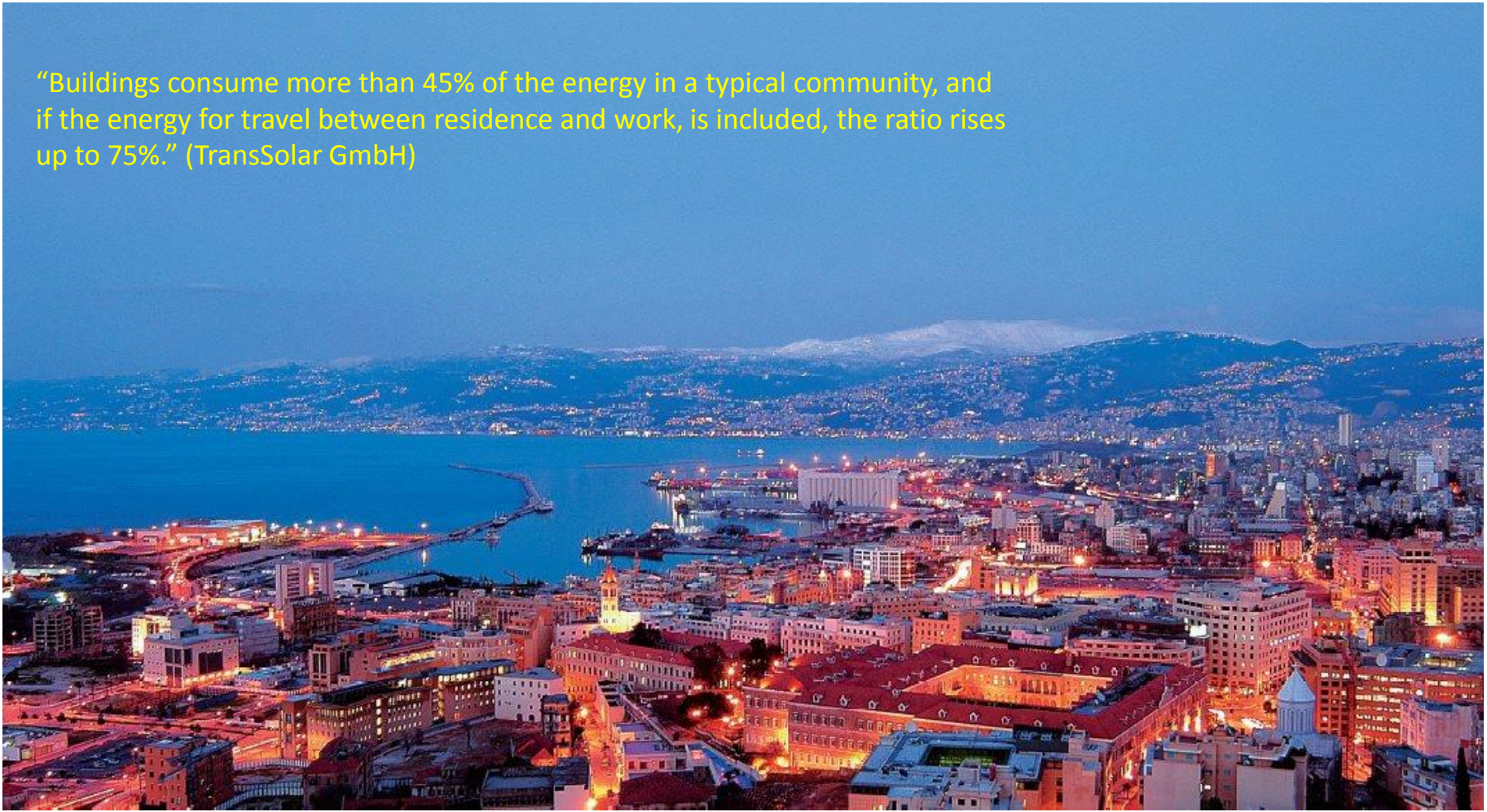
Applying Klima Engineering in an existing school facility in Bekka Valley, Lebanon.

Improving Air Quality and Thermal Comfort through Sustainable and Energy Optimized Measures



By Fadi Charaf
Mentor: Peter Voit
15/09/2014

“Buildings consume more than 45% of the energy in a typical community, and if the energy for travel between residence and work, is included, the ratio rises up to 75%.” (TransSolar GmbH)



Lebanon

Population: 4 Millions

Climatic Conditions: Mediterranean

Area: 10,452 km²



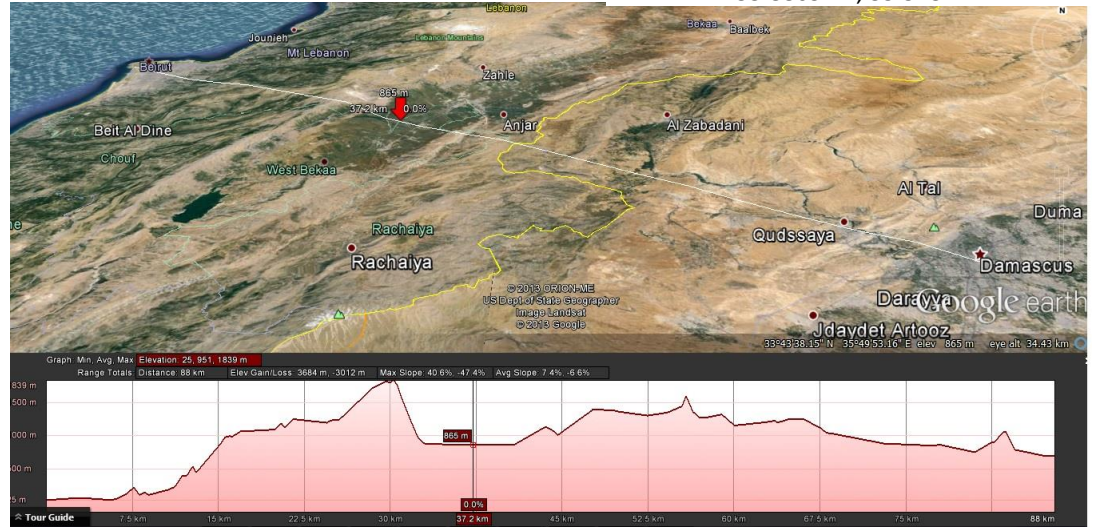
Tri-Arch



Roman Temples 100 BC



Terrain Profile



Modernism



Location

Climate Analysis

The Bekaa valley is an elevated inland plateau (800 m) with different climatic characteristics over the year which includes both a hot arid summer season and a cold winter season.

Outdoor Air Temperature

Minimum Temperature: - 5 °C

Maximum Temperature: 40 °C

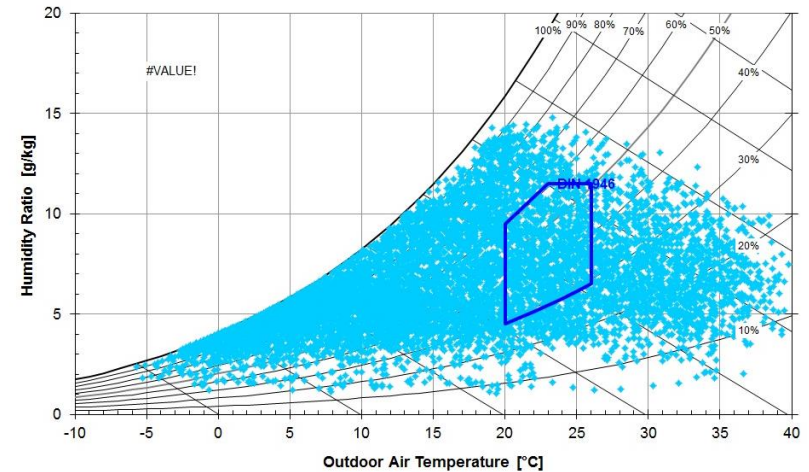
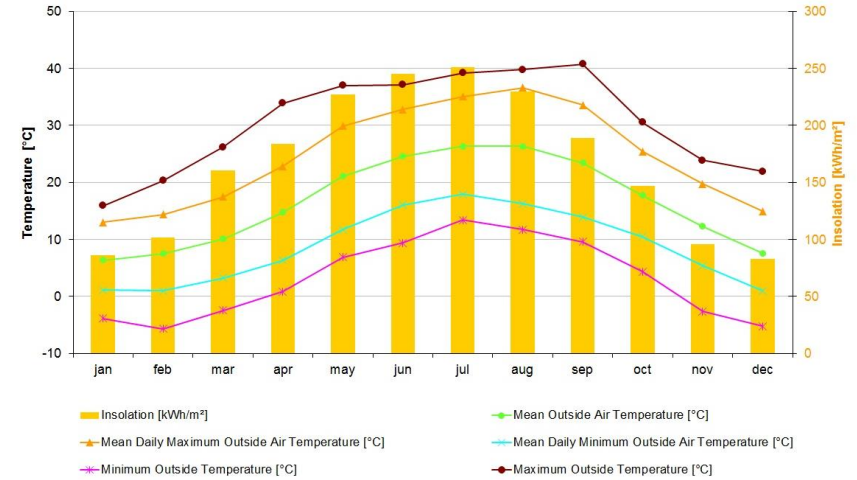
Mean Temperature: 16 °C

Humidity

90% of hours between 7am and 7pm, fall within the recommended humidity threshold of 12 g/kg. Maximum reached absolute humidity is 14 g/kg.

Insolation

High average yearly solar insolation of about 1800 kWh/m².

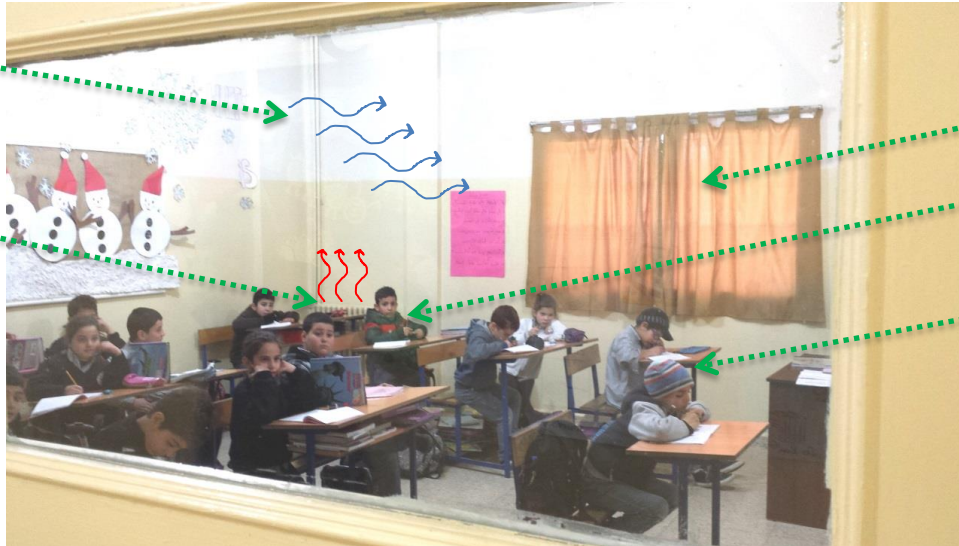


Problem ???

Low thermal comfort and bad air quality during winter time as a result of low and improper heating technique and absence of ventilation.

Heat flux thru
uninsulated wall

Radiators ON



Glare Protection?

Jackets?

Hats?

Agenda

- Analysis:
 - Analyzing Existing Conditions
 - Model Setup for Simulation
 - Codes and Regulations
- Interventions:
 - Improved Conditions
 - Passive Strategies
 - Active Strategies
- Feasibility:
 - Cost Estimation and LCA
- Conclusion and Recommendation

Occupancy

Facility Occupancy

From September till late June

8:00 till 14:30

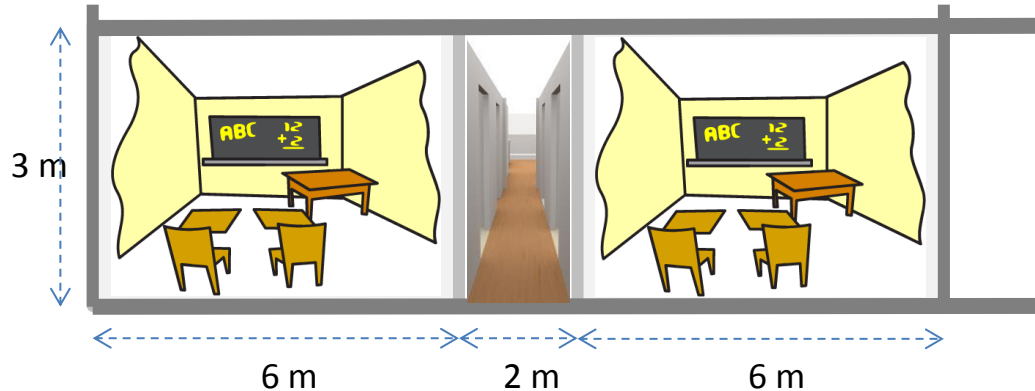
Occupancy= 20 persons/ 36m²

1.8 m²/ person

Main Concern/ First Impression

Dominated by heating, while cooling can be totally achieved by passive strategies

Tuition Fees around 2500 euros/ year

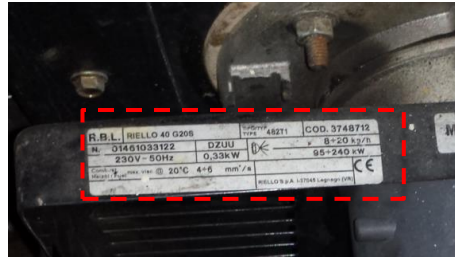


Trnsys Model

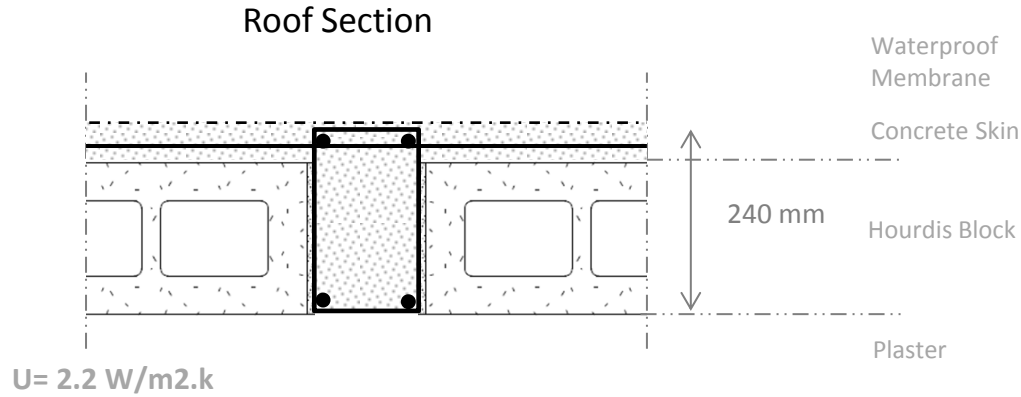
Site Visit

28.01.2014

2 photos per
slide from site
visit, boiler
not necessary

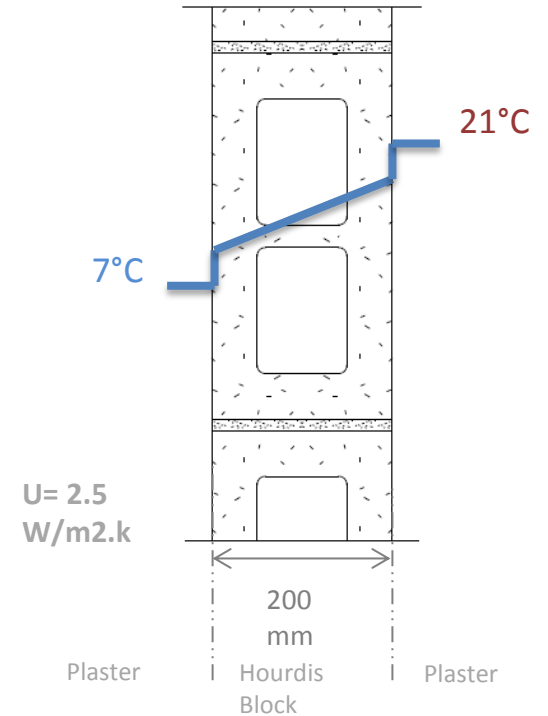


Existing Building Envelope

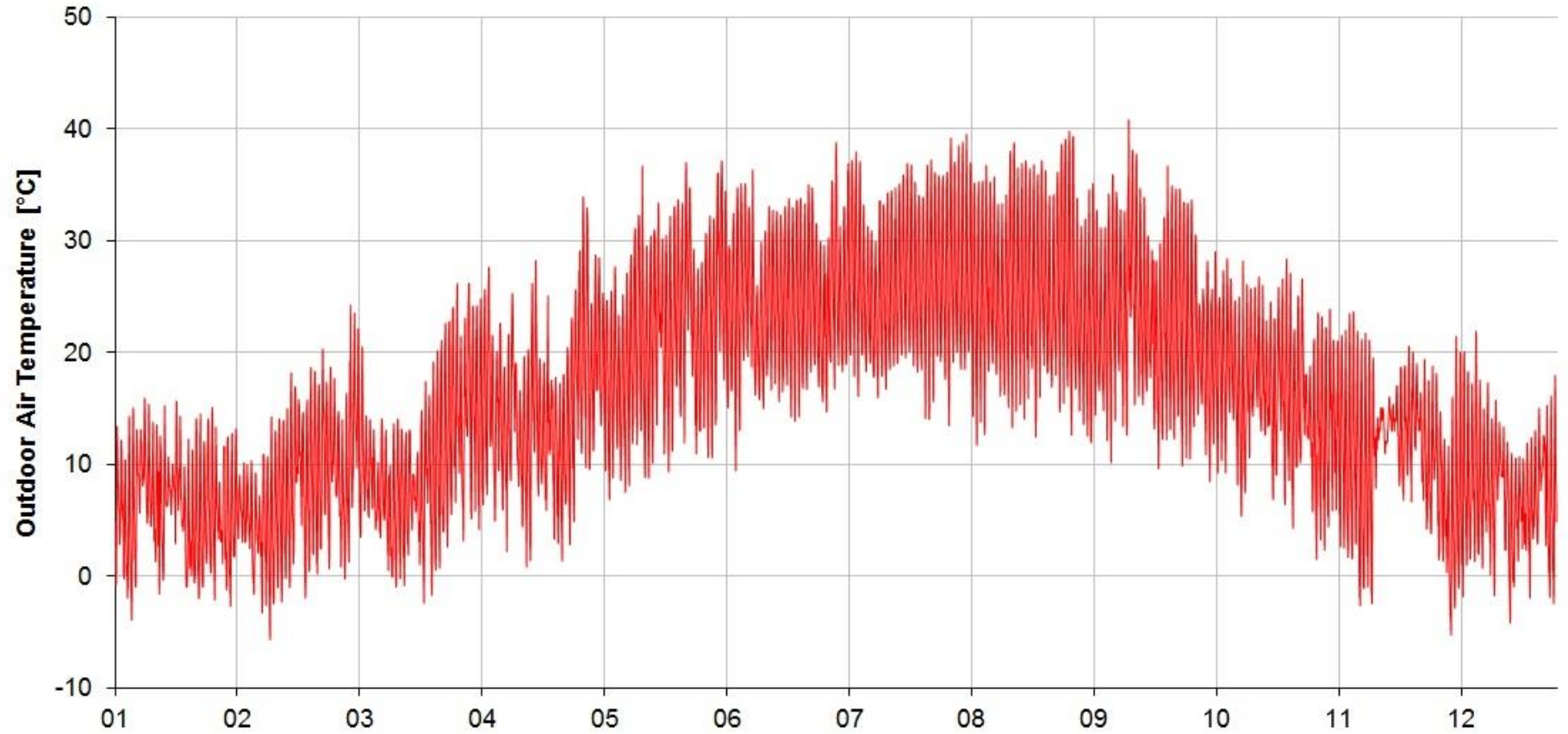


Wall Section

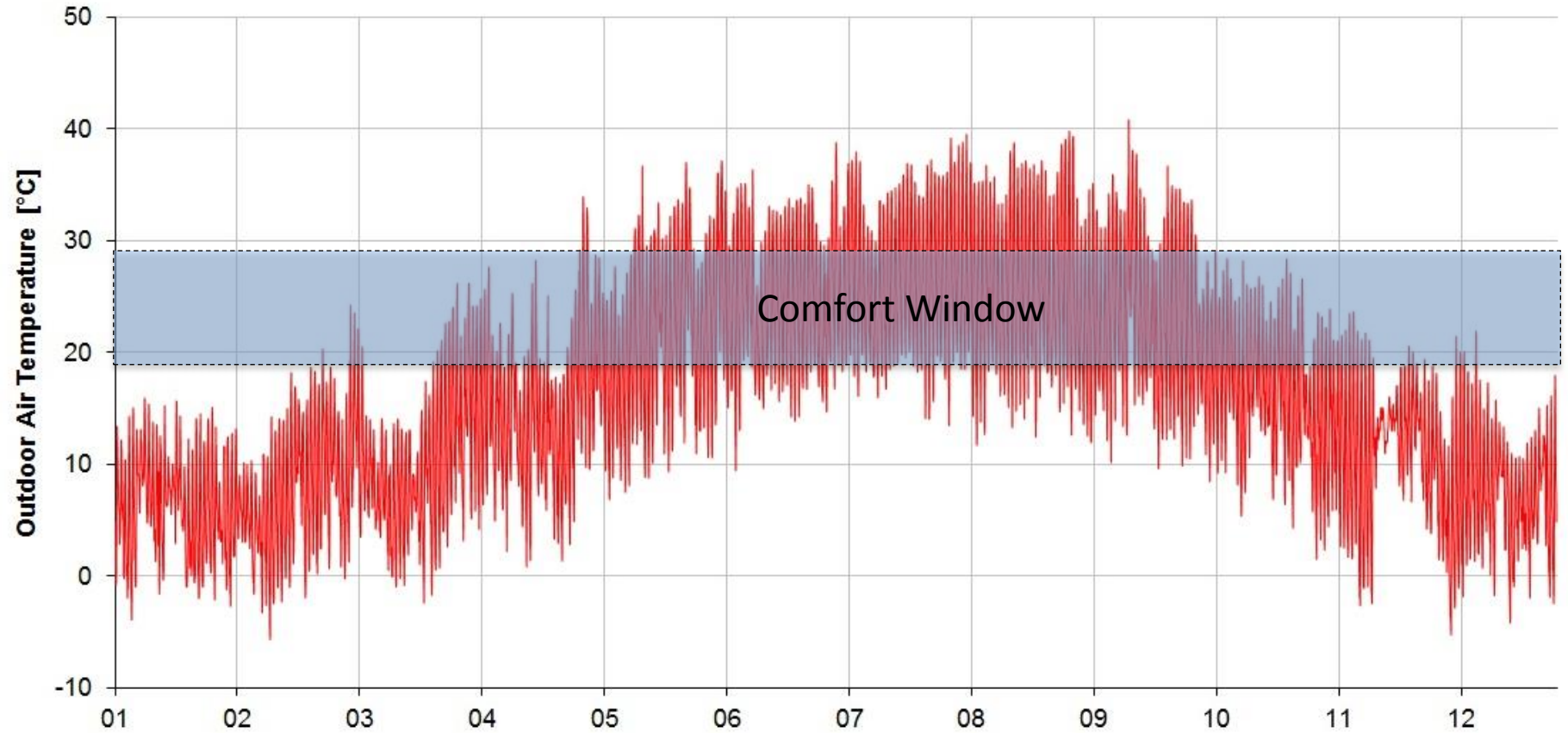
$Q = 35 \text{ W/m}^2$



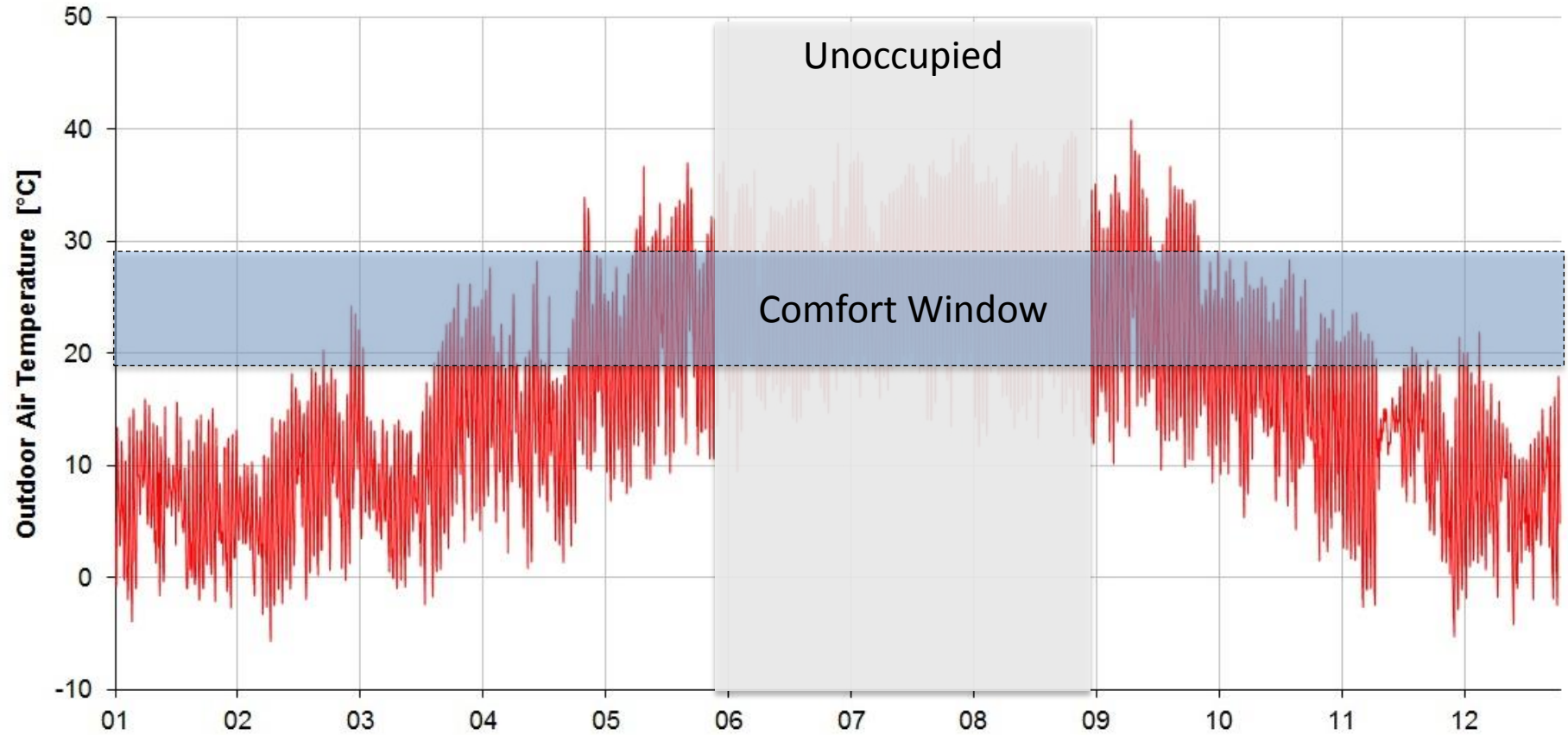
Ambient Temperature



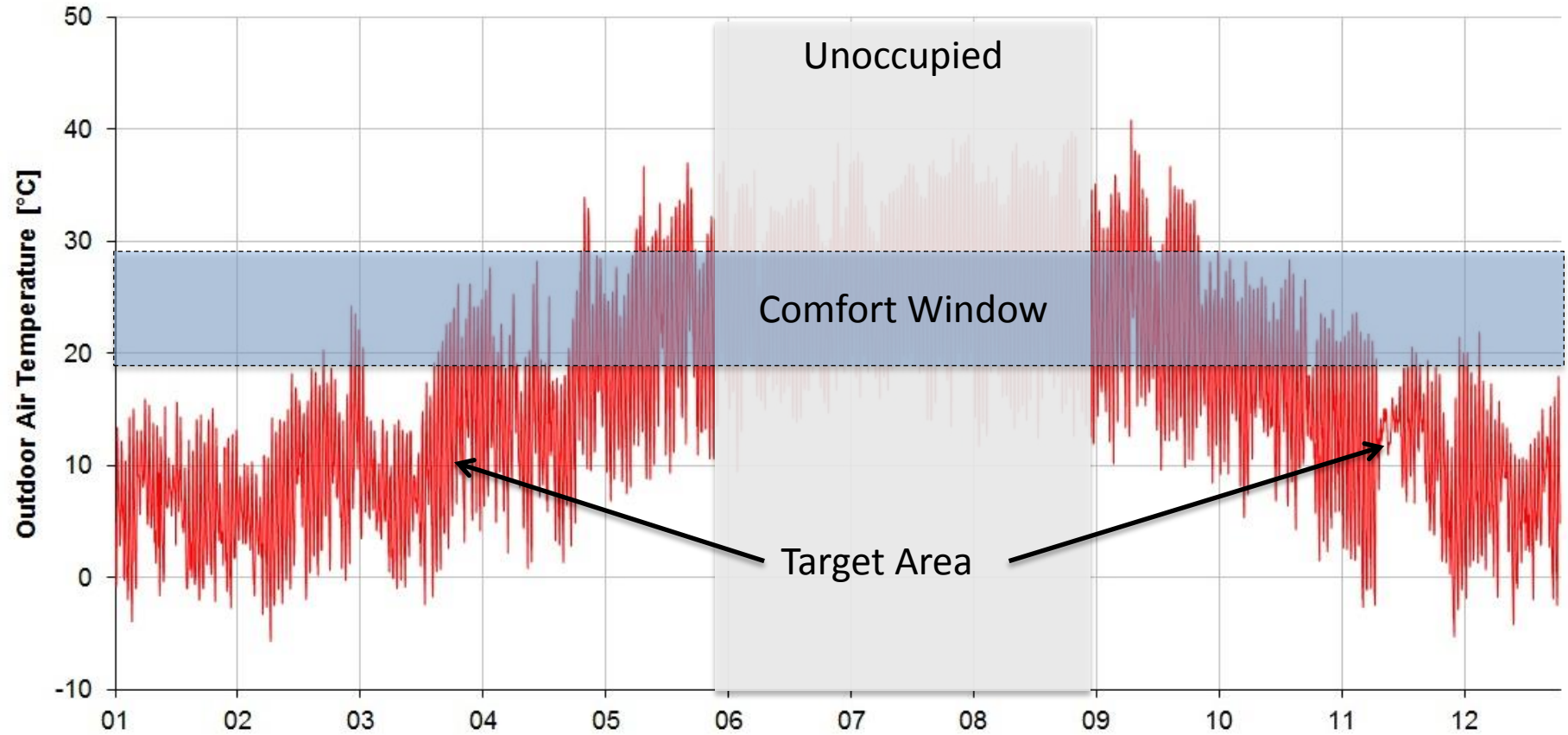
Annual Comfort



Annual Comfort



Annual Comfort

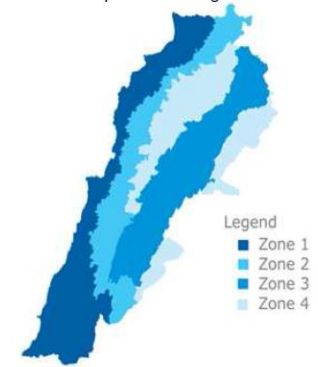


Target Level Assessment

- ✓ DIN 15251
- ✓ ASHRAE 62.1
- ✓ THERMAL STANDARD FOR BUILDINGS IN LEBANON

Table 2: General characteristics of climate zones and sub-zones

Climatic Zone	Climatic Sub-zone	Winter	Summer	Daily Gap
1 Coastal	1A Altitude < 400 m	Warm and short	Hot and humid	Small all year
	1B Altitude > 400 m	Cold and long increasing with altitude	Hot and humid with maximum daily temperatures differing slightly from 1A	
2 Western Mid Mountain	No Sub-zone	Cold and long increasing with altitude	Cool and Moderate summer	More pronounced than the daily gap of zone 1
3 Inland Plateau	No Sub-zone	Colder and longer than the winter at same altitudes in zones 1 & 2 (min temperatures lower than zones 1 & 2)	Hot and dry summer, but cool at night. The min temperatures are lower than zones 1 & 2 and the max temperatures are higher. Very low humidity.	In summer the daily gap is high and varies according to the year.
4 High Mountain	No Sub-zone	Long and rigorous	Cool	Moderate to high in Eastern Mountain



Building Envelon

Table 3: Reference Thermal Transmittance Values per Component U-ref (W/m².K) vs. climatic zone

Climatic Zone	Building category	U-value Roof	U-value Wall	U-value Window & Skylight	U-value Ground Floor	
					Exposed*	Semi-exposed**
1 Coastal	1 Residential	0.71	1.60	5.80	1.70	2.00
	2 N Residential	0.71	1.26	5.80	1.70	2.00
2 Mid Mountain	1 Residential	0.63	0.77	4.00	0.77	1.20
	2 N Residential	0.55	0.65	3.30	0.70	1.20
3 Inland Plateau	1 Residential	0.63	0.77	4.00	0.77	1.20
	2 N Residential	0.55	0.65	3.30	0.70	1.20
4 High Mountain	1 Residential	0.55	0.57	3.30	0.66	1.00
	2 N Residential	0.55	0.57	2.60	0.66	1.00

TABLE 6-1 MINIMUM VENTILATION RATES IN BREATHING ZONE
(This table is not valid in Isolation; it must be used in conjunction with the accompanying notes.)

Occupancy Category	People Outdoor		Area Outdoor		Notes	Default Values			Air Class
	Air Rate		Air Rate			Occupant Density	Combined Outdoor		
	R _p	R _a	R _p	R _a		(see Note 4)	Air Rate (see Note 5)		
	cfm/person	L/s/person	cfm/ft ²	L/s/m ²		#/1000 ft ² or #/100 m ²	cfm/person	L/s/person	
Correctional Facilities									
Cell	5	2.5	0.12	0.6		25	10	4.9	2
Dayroom	5	2.5	0.06	0.3		30	7	3.5	1
Guard stations	5	2.5	0.06	0.3		15	9	4.5	1
Booking/waiting	7.5	3.8	0.06	0.3		50	9	4.4	2
Educational Facilities									
Daycare (through age 4)	10	5	0.18	0.9		25	17	8.6	2
Daycare sickroom	10	5	0.18	0.9		25	17	8.6	3
Classrooms (ages 5-8)	10	5	0.12	0.6		25	15	7.4	1
Classrooms (age 9 plus)	10	5	0.12	0.6		35	13	6.7	1

- Temperature

Class A: Heating: 21°C ; Cooling: 25°C

Range 18 °C < Top < 28°C

- Indoor Air Quality

ASHRAE 60.1: 5 L/s/pseron *20 persons= 360m³/h or 3.3 ACH

Remove graphs

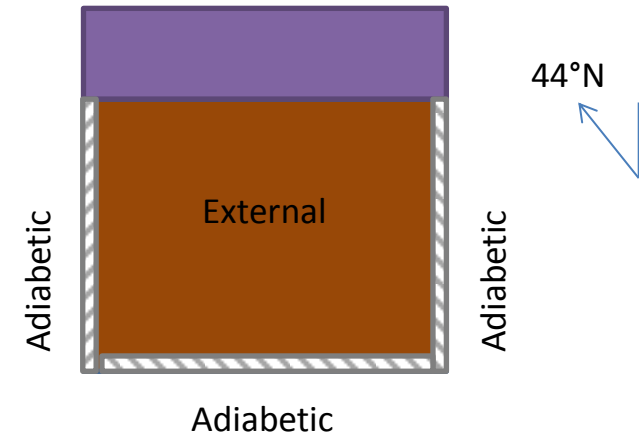
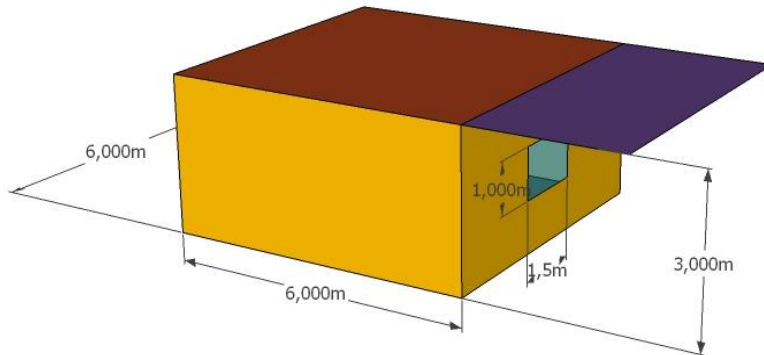
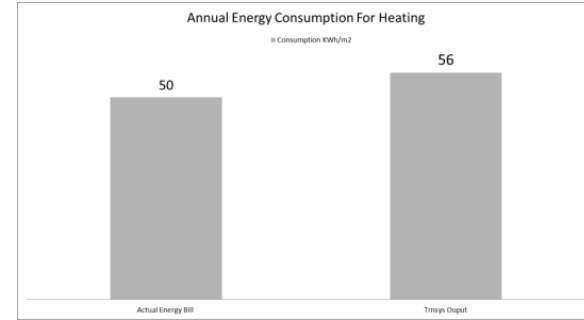
ShoeBox Model - Trnsys

Infiltration 0.3 ACH (operation) + 0.1 ACH

Gains 20 Students seated (100 Watts – Sensible + Latent)

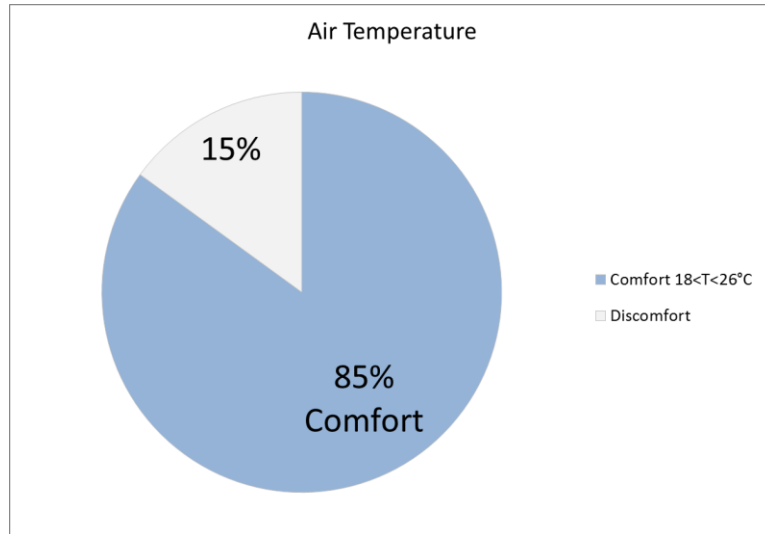
Shoebox Dimensions (6 × 6 × 3m typical measured classroom)

Operation Mode: from 07:00 till 14:00 (except for Weekend)

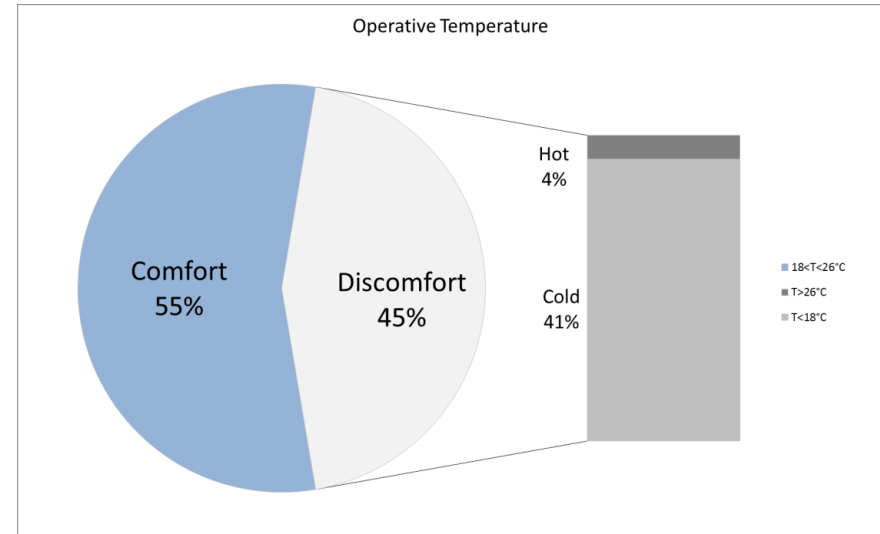


Existing Conditions (including Heating)

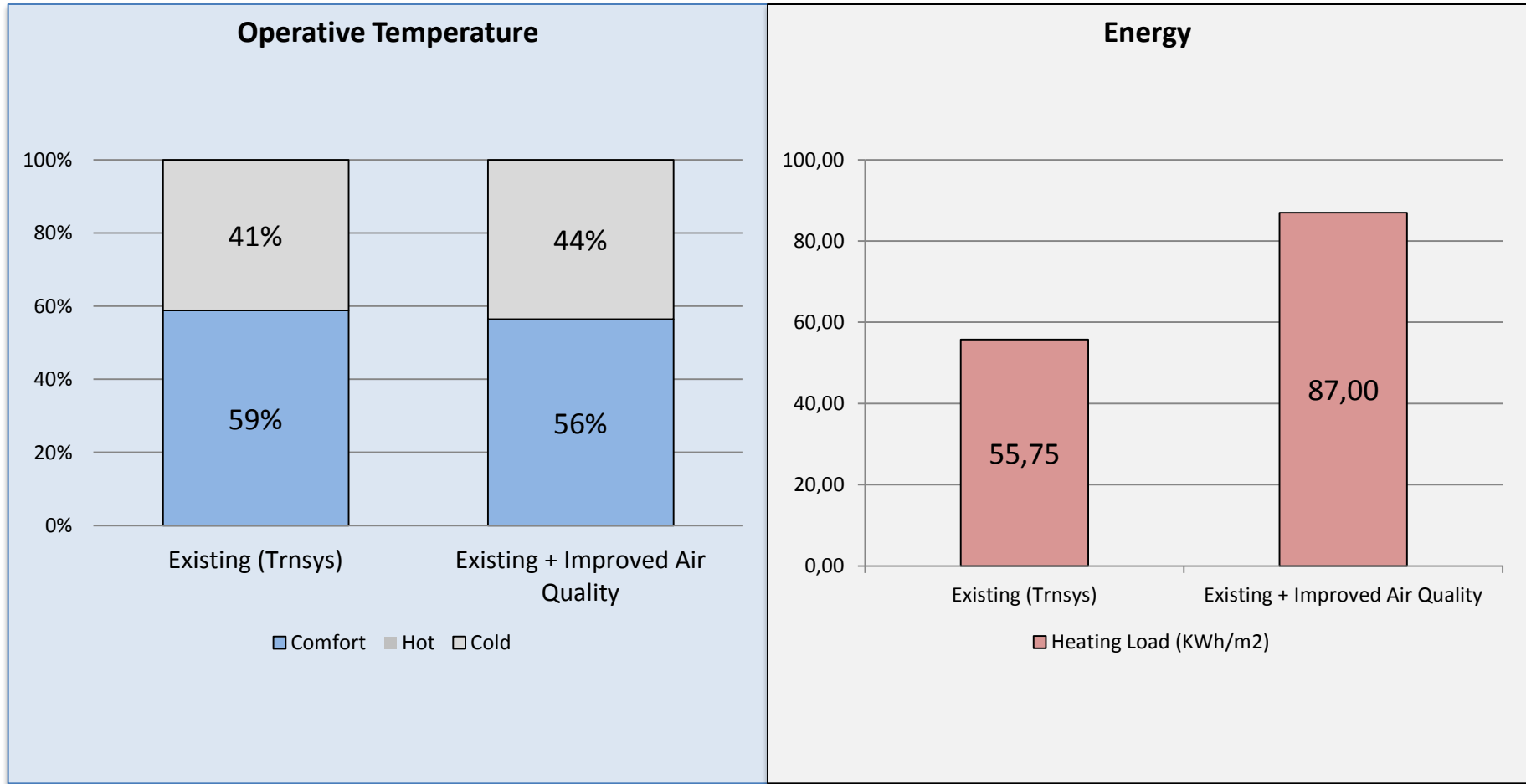
Air



Perceived

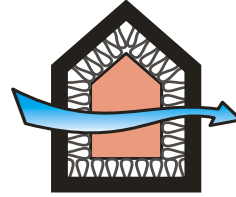


Improved Air Quality + Heating

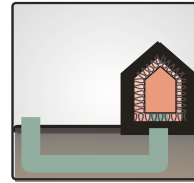


Passive Strategies

- Insulated – Reference Case



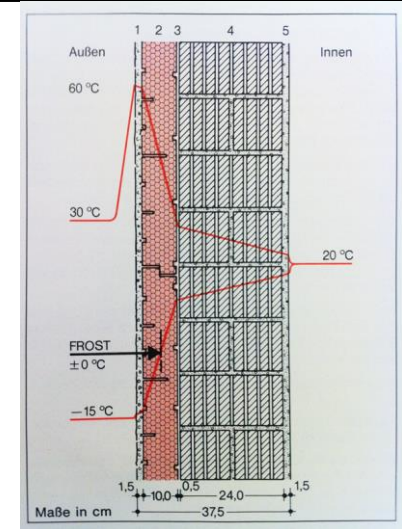
- Ground Duct + Insulation



Passive Strategies

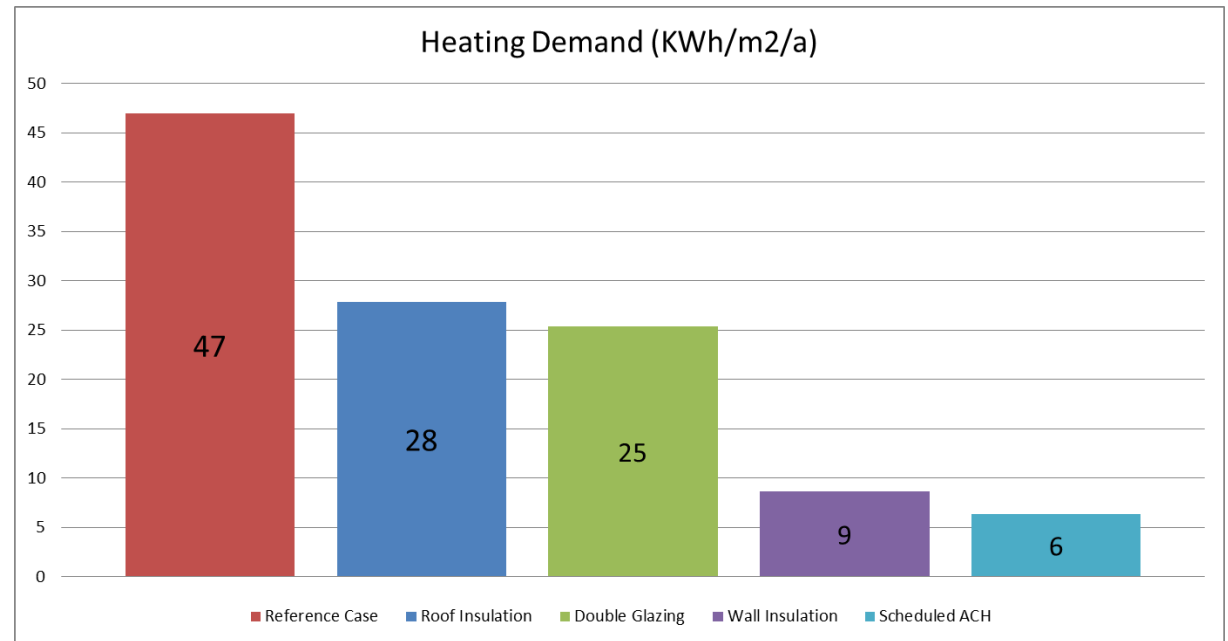
- Insulated – Reference Case

- Type EPS W040
- Thickness:
 - Walls: 10 cm
 - Roof 15 cm

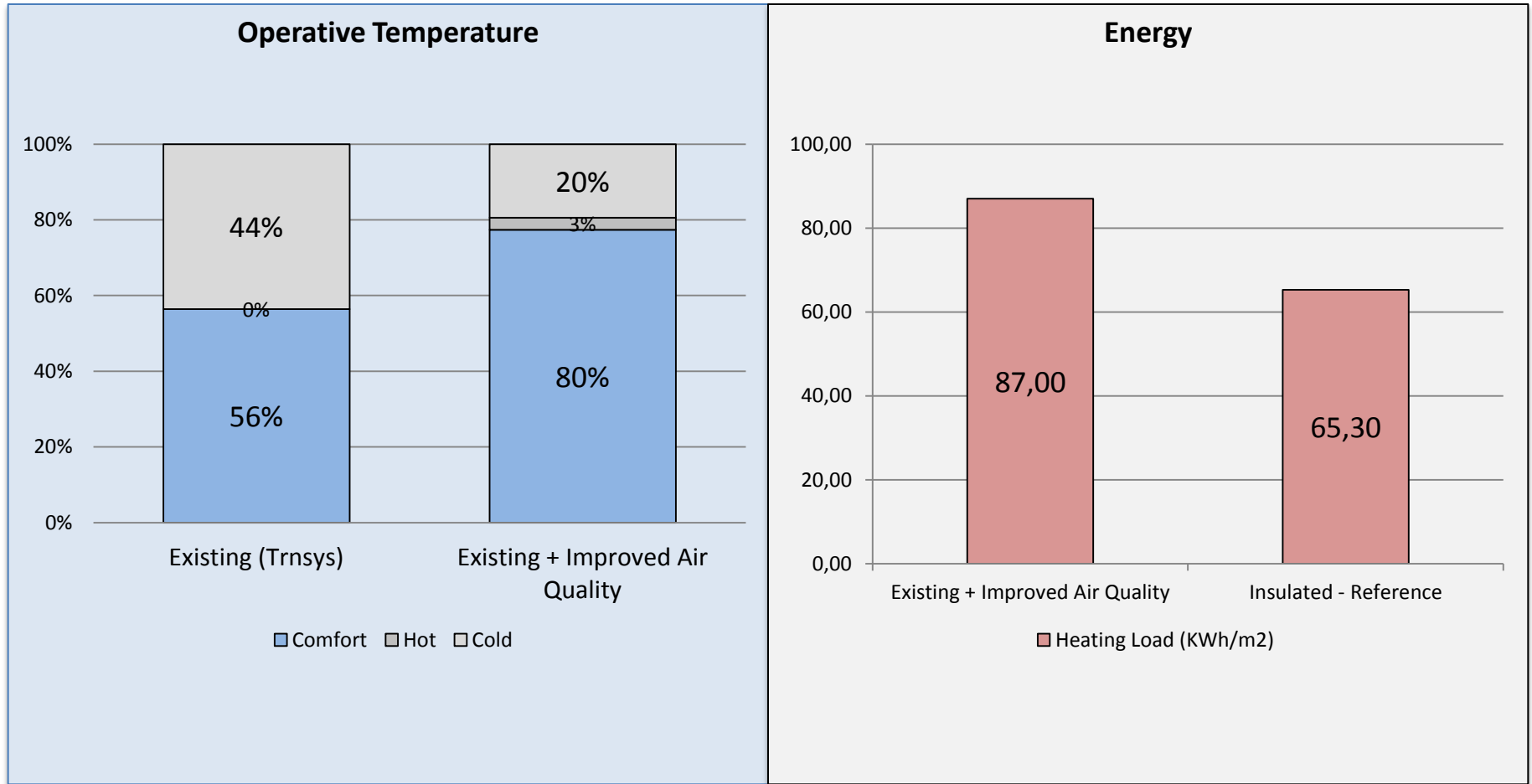


Insulated – Reference Case

The effect of each insulated element on annual heating load in the absence of proper ventilation



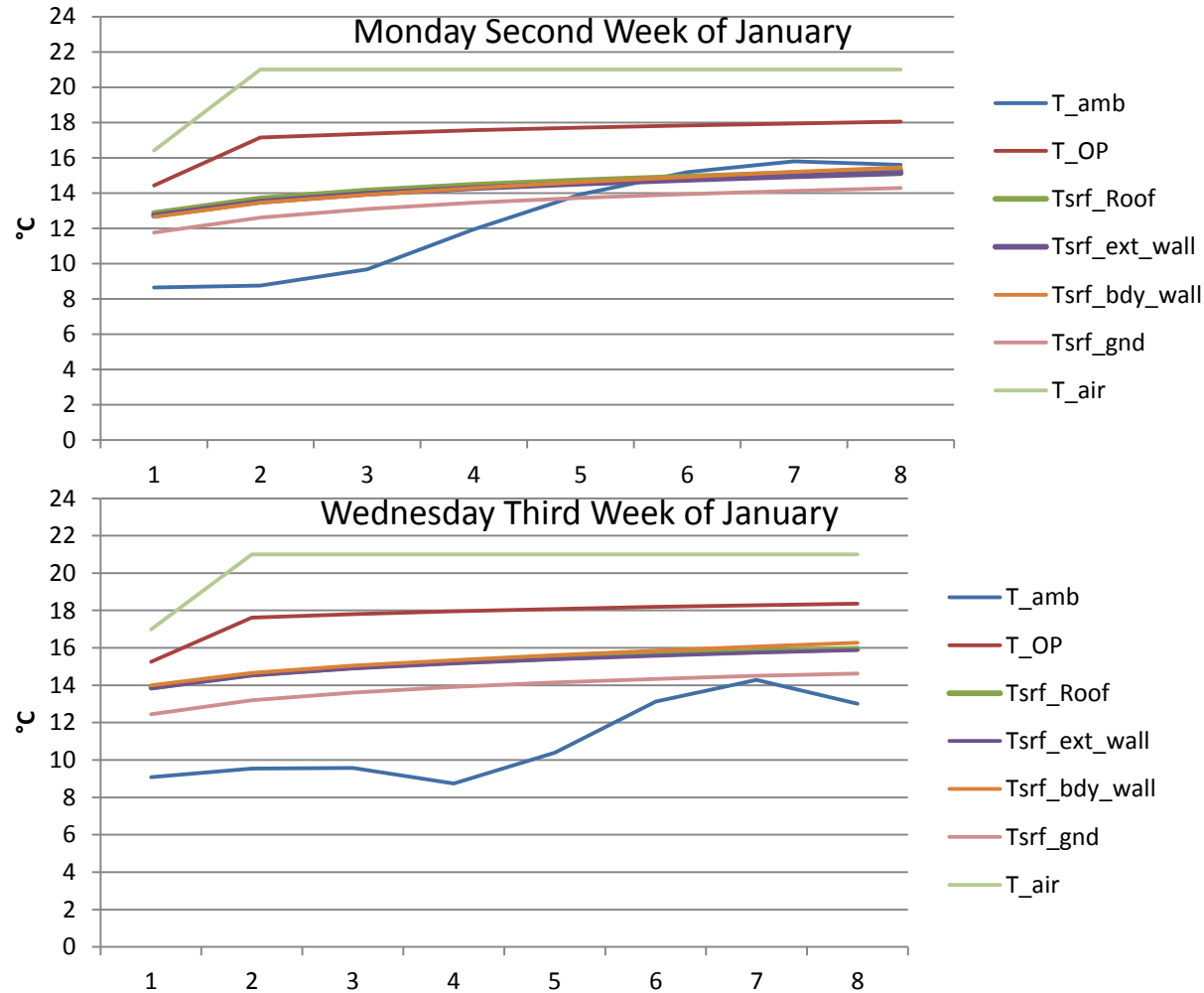
Insulation – Reference Case



Insulated – Reference Case

Thermal Mass Heat Storage over the day

- Monday colder surfaces stored from weekend
- Wednesday hotter surfaces from the day before

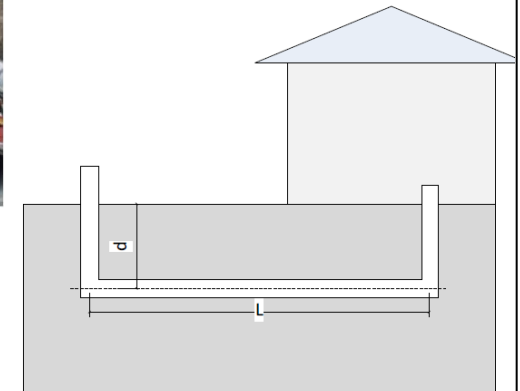


Passive Strategies

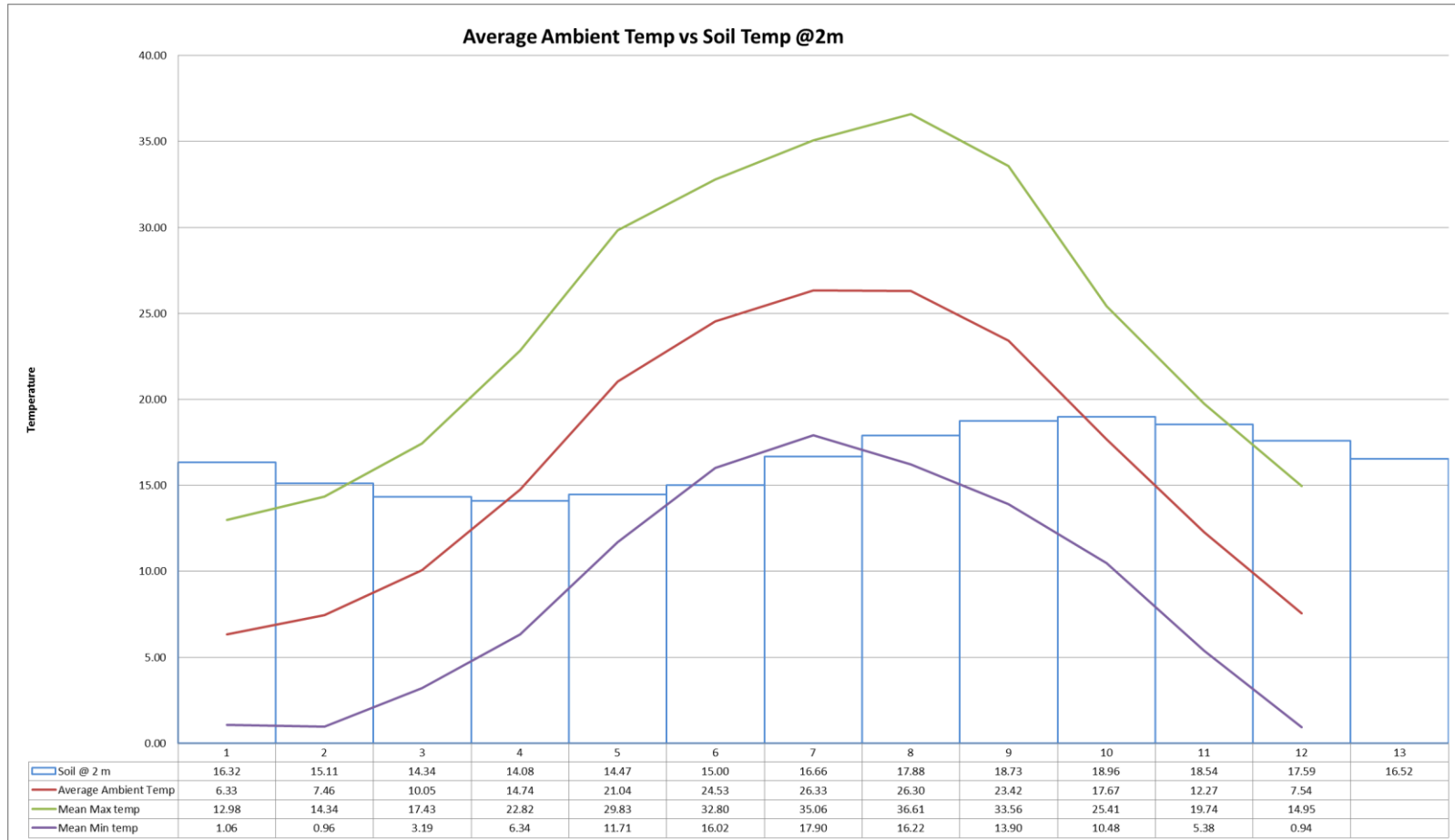
– Insulated – Reference Case

– Ground Ducts + Insulation

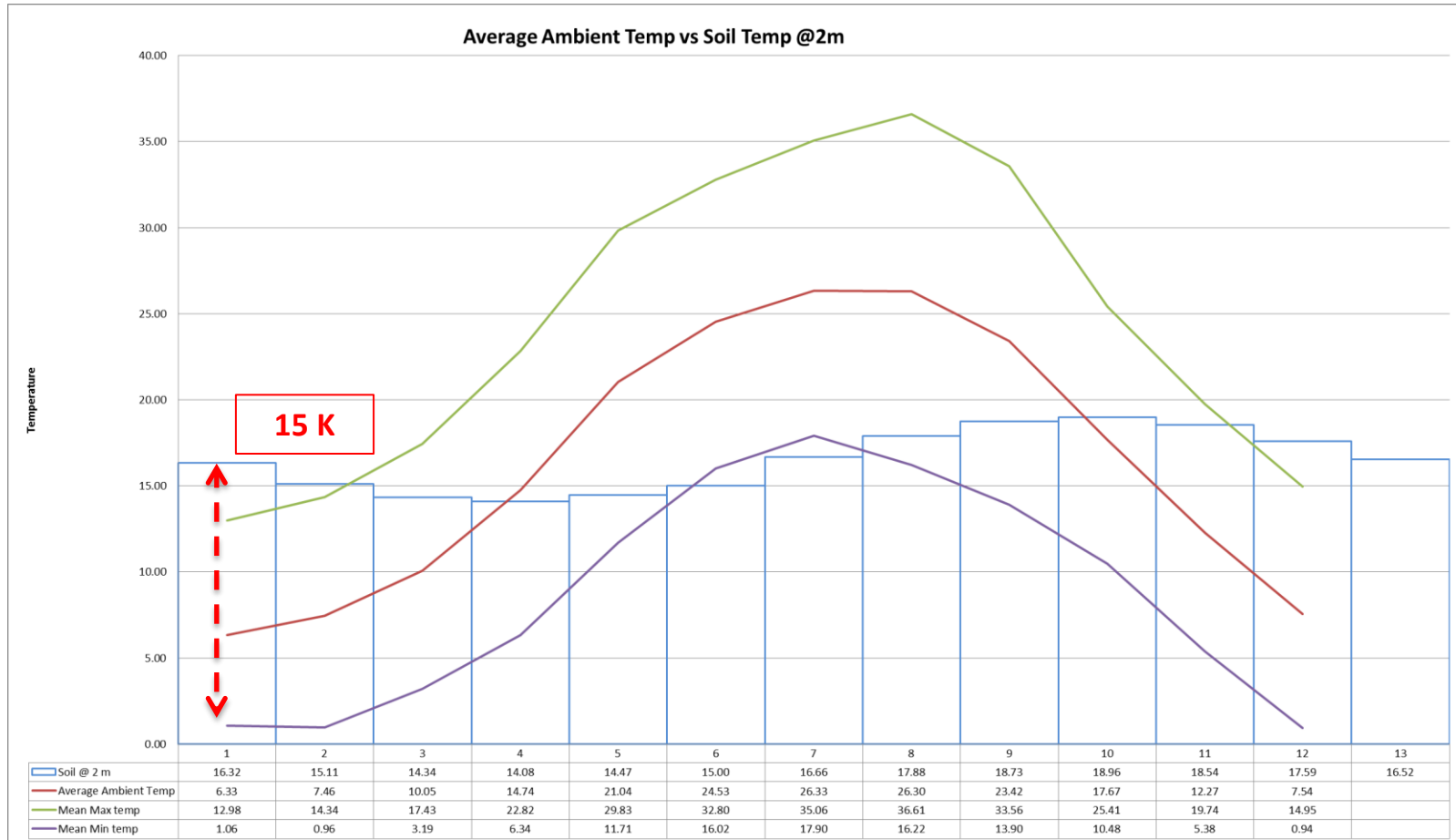
- Insulation:
 - Type EPS (0.04 W/mK)
 - Thickness:
 - Walls: 10 cm
 - Roof 15 cm
- Ground Ducts:
 - Reinforced Concrete Pipes
 - Length 100 m, Diameter 1 m, Thickness 10cm



Ground Ducts + Insulation



Ground Ducts + Insulation



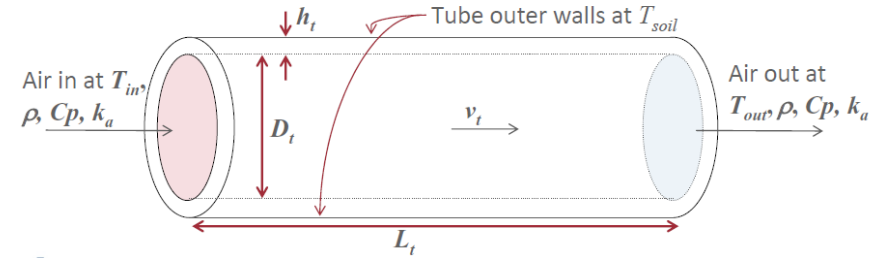
Ground Ducts + Insulation

Efficiency of Heat Recovery 75%

Operation @ $T_{duct} > T_{amb}$

Assumption: $T_{wall} = T_{soil}$

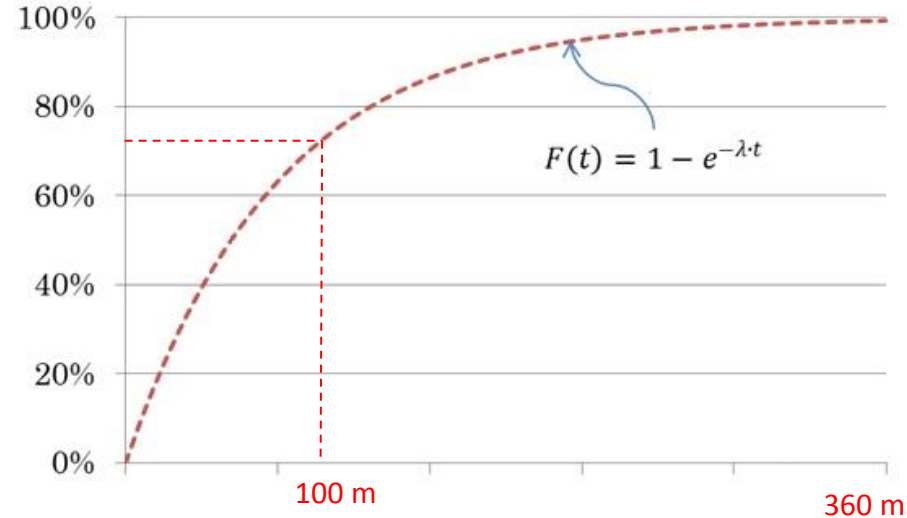
Neglect the Resistance of Wall (10cm concrete)



$$Nu_o = \frac{\left(\frac{f}{8}\right) (Re - 1000) Pr}{1 + 12.7 \left(\frac{f}{8}\right)^{0.5} (Pr^{\frac{2}{3}} - 1)} \left[1 + \left(\frac{D}{L}\right)^{\frac{2}{3}} \right]$$

where $f = (0.790 \ln Re - 1.64)^{-2}$

$$T_{out} = T_{soil} + (T_{in} - T_{soil}) e^{-\frac{\pi D_t L_t U_t}{v_t \rho C_p}}$$



Tool for Ground Duct Heat Recovery

1. Turbulent Flow Inside a Circular Tube									
Inputs			Calculation						
Fluid = air			Reynolds Number, Re = 140,845						
Ave. Fluid Temp, T _s = 7 °C			For: 0.7 < Pr < 120 10,000 < Re < 160,000 L/D > 10 (50 ?)						
Duct Properties			Prandtl Number, Pr = 0.7						
B = 0.75 m									
Area m ² = 0.5625									
Hydraulic Diam d _s = 4 A / P = 1			Correlation #1, the Dittus Boelter Correlation						
Wetted Perimeter P = d + 2 = 2.25			Correlation #1, the Dittus Boelter Correlation						
Rectangular section									
Wall Thickness = 0.1 m			T _{wall} > T _{fluid} Nu _s = 284						
Circular			Nu _s = 0.023 Re ^{0.8} Pr ^{0.4} for T _{wall} > T _{fluid}						
Pipe Diam, D = 1000 mm			h _s = 24 kJ/hr-m ² -K						
			Nu _s = 0.02 Re ^{0.8} Pr ^{0.3} for T _{wall} < T _{fluid}						
Pipe Diam, D = 1.000 m			h _s = 7 W/m ² -K						
Surface Roughness ε = 0.0005 m			T _{wall} > T _{fluid} Nu _s = 309						
Thermal Conductivity of = 1 W/m·K			Correlation #2, Gnielinski Correlation, Conv						
Fluid Properties			h _s = 28 kJ/hr-m ² -K						
Avg flow = 1.5707963 m ³ /s			f = 0.01675						
Avg flow = 4050 m ³ /hr									
Ave. Velocity, V = 2 m/s			Correlation #2:						
Fluid Density, ρ = 1.25 kg/m ³			Nu _s = 237						
Fluid viscosity, μ = 1.775E-05 kg/m·s			h _s = 21 kJ/hr-m ² -K						
Fluid Sp. Heat, C _p = 1.005 kJ/kg·K			h _s = 6 W/m ² -K						
Fluid Thermal Conductivity, k = 0.025 W/m·K			Correlation #3: looks more realistic						
Fluid Thermal Conductivity, k = 0.000025 kJ/s-m·K			Nu _s = 237						
Fluid Thermal Conductivity, k = 0.09 kJ/hr-m·K			h _s = 21 kJ/hr-m ² -K						
Pipe Length, L = 400 m			Correlation #4: Convection H.T., Turb. Pipe						
			Nu _s = #NUM!						

$$Nu = \frac{h D}{k} \quad Re = \frac{D V \rho}{\mu}$$

$$Pr = \frac{v}{\alpha} = \frac{\mu C_p}{k}$$

Dimensionless Numbers used in Forced Convection Heat Transfer Coefficient Correlations

For: 0.7 < Pr < 120
10,000 < Re < 160,000
L/D > 10 (50 ?)

$$Nu_s = 0.023 Re^{0.8} Pr^{0.4} \text{ for } T_{wall} > T_{fluid}$$

$$Nu_s = 0.02 Re^{0.8} Pr^{0.3} \text{ for } T_{wall} < T_{fluid}$$

Approach 1 Temperature Calculation			
Trial	Input		Tout
56	Tsoil	15 °C	12.32
57	Tin	15 °C	
58	Length of Duct	100 m	
59	Pie	3.1415927	Efficiency 73.16%

$$Nu_s = \left(\frac{f}{8} \right) (Re - 1000) Pr$$

$$1 + 12.7 \left(\frac{f}{8} \right)^{0.5} (Pr^{\frac{1}{4}} - 1)$$

where $f = (0.790 \ln Re - 1.64)^{-2}$

Approach 2 U value including hc and wall conductivity			
U	2.180544 W/m ² -K	With U _s Considered	Tout 8.862318548
U _s	7.9053999 KJ/hr-m ² -K		

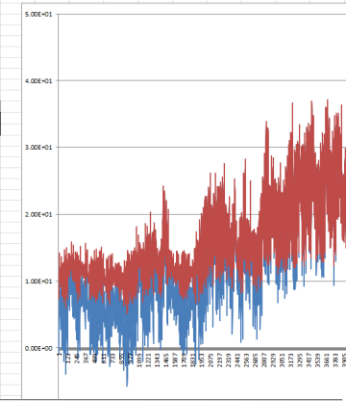
$$Nu_s = \left(\frac{f}{8} \right) (Re - 1000) Pr$$

$$1 + 12.7 \left(\frac{f}{8} \right)^{0.5} (Pr^{\frac{1}{4}} - 1)$$

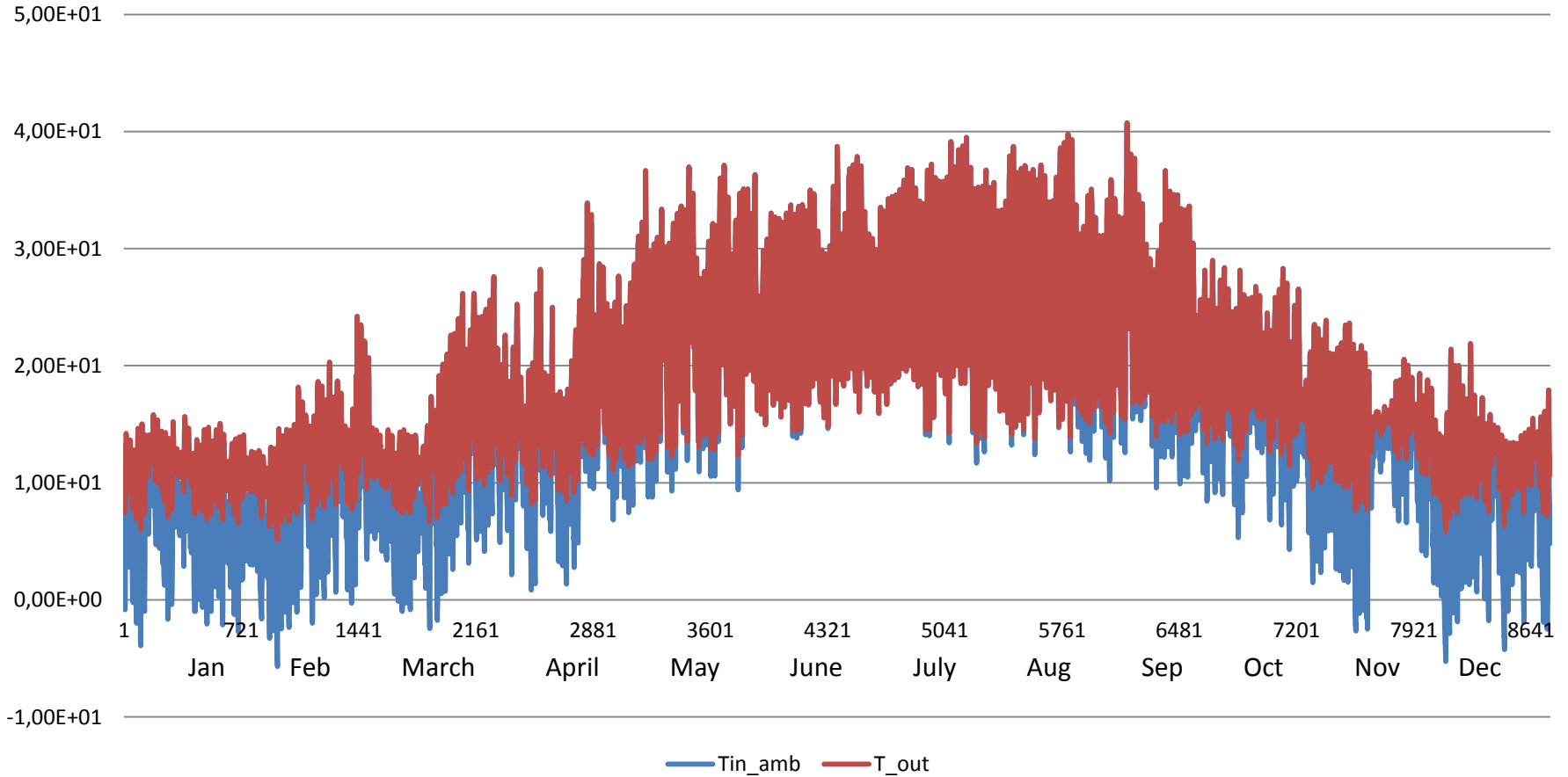
where $f = (0.790 \ln Re - 1.64)^{-2}$

PART 1 Temp									
Operation	T_amb	Tamb,Op	Month	Tsoil	Tout	ΔT	Tsoil-Tin	T duct output	Watts (mcl)
81	0	3.55E+00	0.00	1	15.00				9.53
82	0	2.36E+00	0.00	1	15.00				8.97
83	0	1.47E+00	0.00	1	15.00				8.55
84	0	8.94E-01	0.00	1	15.00				8.20
85	0	1.59E-01	0.00	1	15.00				7.91
86	0	-5.50E-01	0.00	1	15.00				7.58
87	1	-8.43E-01	-0.84	1	15.00	7.4403929	8.28	15.84	7.44
88	1	-2.94E-01	-0.17	1	15.00	7.7167056	7.99	15.27	7.71
89	1	7.53E-01	0.75	1	15.00	8.202583	7.45	14.25	8.20
90	1	3.41E+00	3.41	1	15.00	9.4688749	6.06	11.59	9.47
91	1	7.17E+00	7.17	1	15.00	11.202318	4.10	7.83	11.26
92	1	1.00E+01	10.00	1	15.00	12.81418	2.61	5.00	12.81
93	1	1.20E+01	12.00	1	15.00	13.568508	1.57	3.00	13.57
94	1	1.34E+01	13.38	1	15.00	14.224009	0.85	1.63	14.22
95	0	1.25E+01	0.00	1	15.00				13.81
96	0	1.13E+01	0.00	1	15.00				13.39
97	0	1.05E+01	0.00	1	15.00				12.85
98	0	9.95E+00	0.00	1	15.00				12.38
99	0	8.44E+00	0.00	1	15.00				11.87
100	0	7.94E+00	0.00	1	15.00				11.63
101	0	8.06E+00	0.00	1	15.00				11.69
102	0	7.54E+00	0.00	1	15.00				11.45
103	0	6.44E+00	0.00	1	15.00				10.91
104	0	5.94E+00	0.00	1	15.00				10.68
105	0	6.00E+00	0.00	1	15.00				10.71
106	0	6.00E+00	0.00	1	15.00				10.71

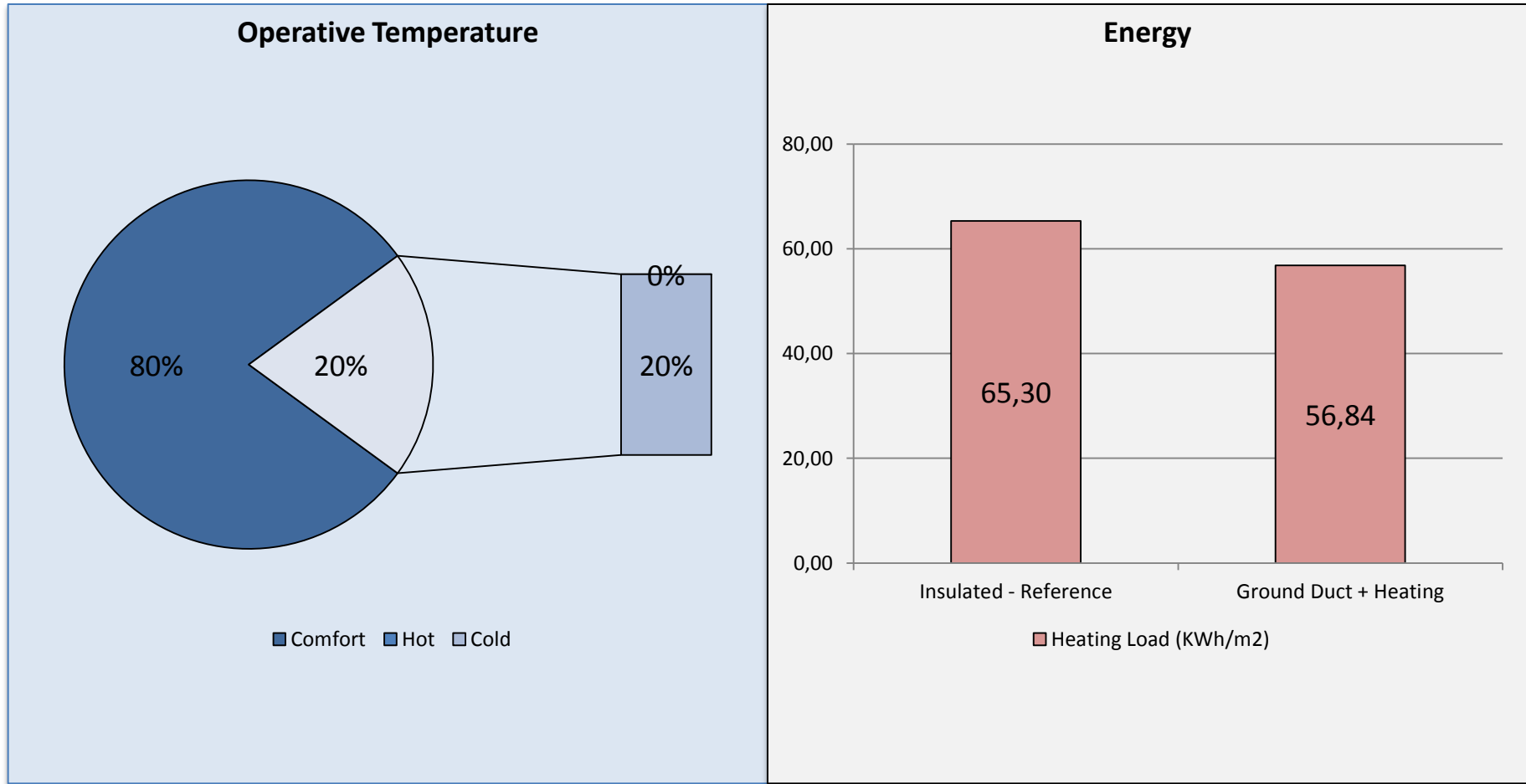
Energy used
6006.90 kWh
13.90 kWh/m²



Ground Ducts + Insulation

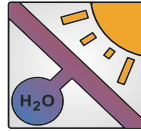


Ground Ducts + Insulation



Active Strategies

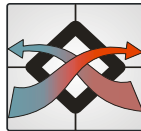
- Solar Thermal Collector



- PV + Heat pump



- AHU



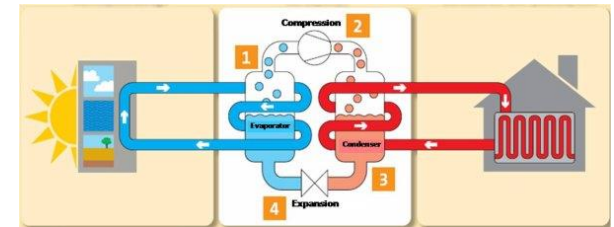
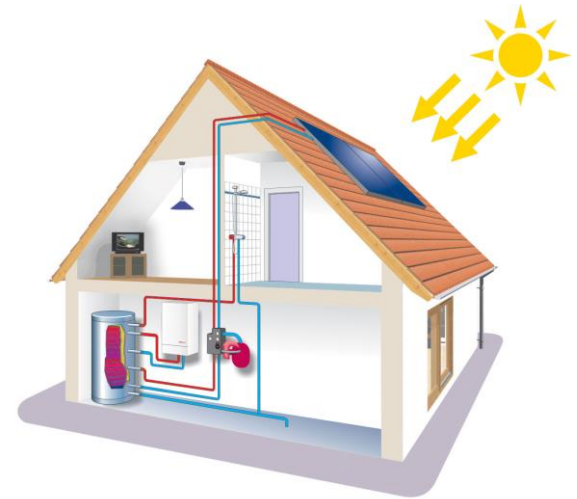
- Solar Air Collector



Active Strategies

- Solar Thermal Collector
- PV + Heat pump
- AHU
- Solar Air Collector

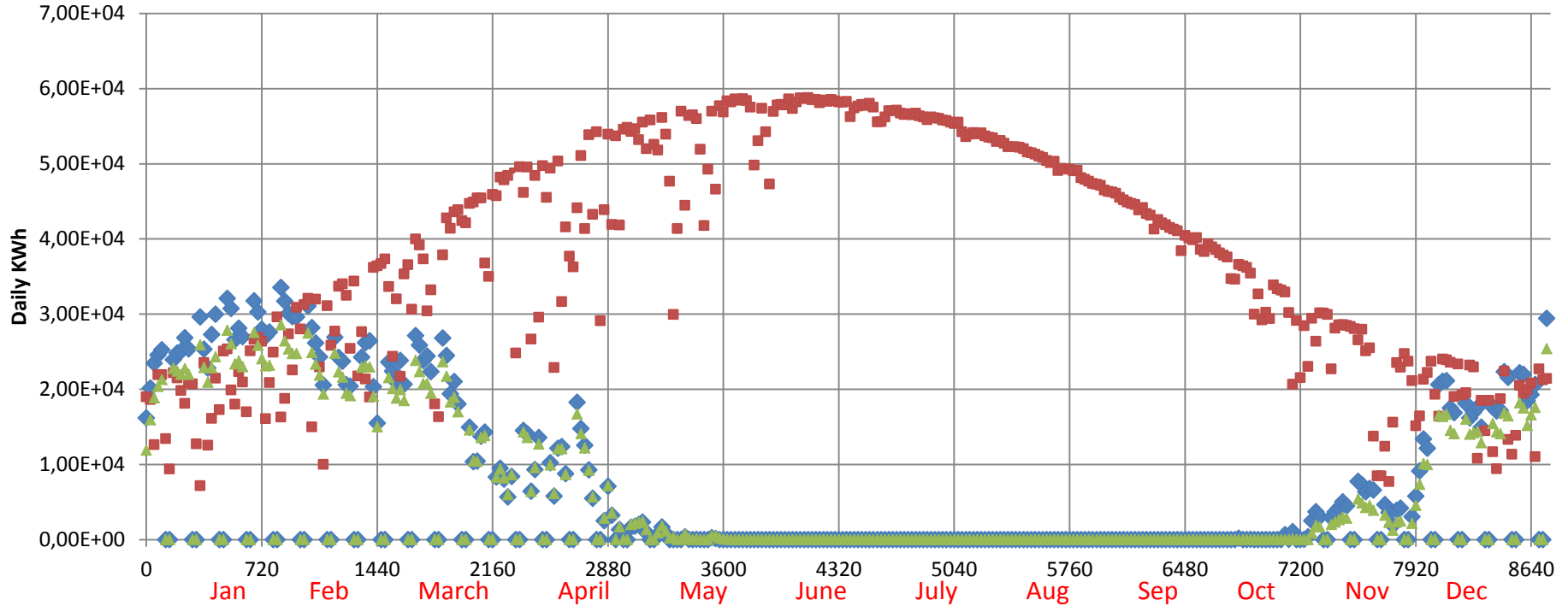
- Radiator Connected to Solar Thermal Plant 10m².
- Heat output is related to the average montinored demand during heating season.
- Boiler Set to 70°C



Solar Thermal - Primary Investigation

Horizontal Surface Output vs Heating Demand

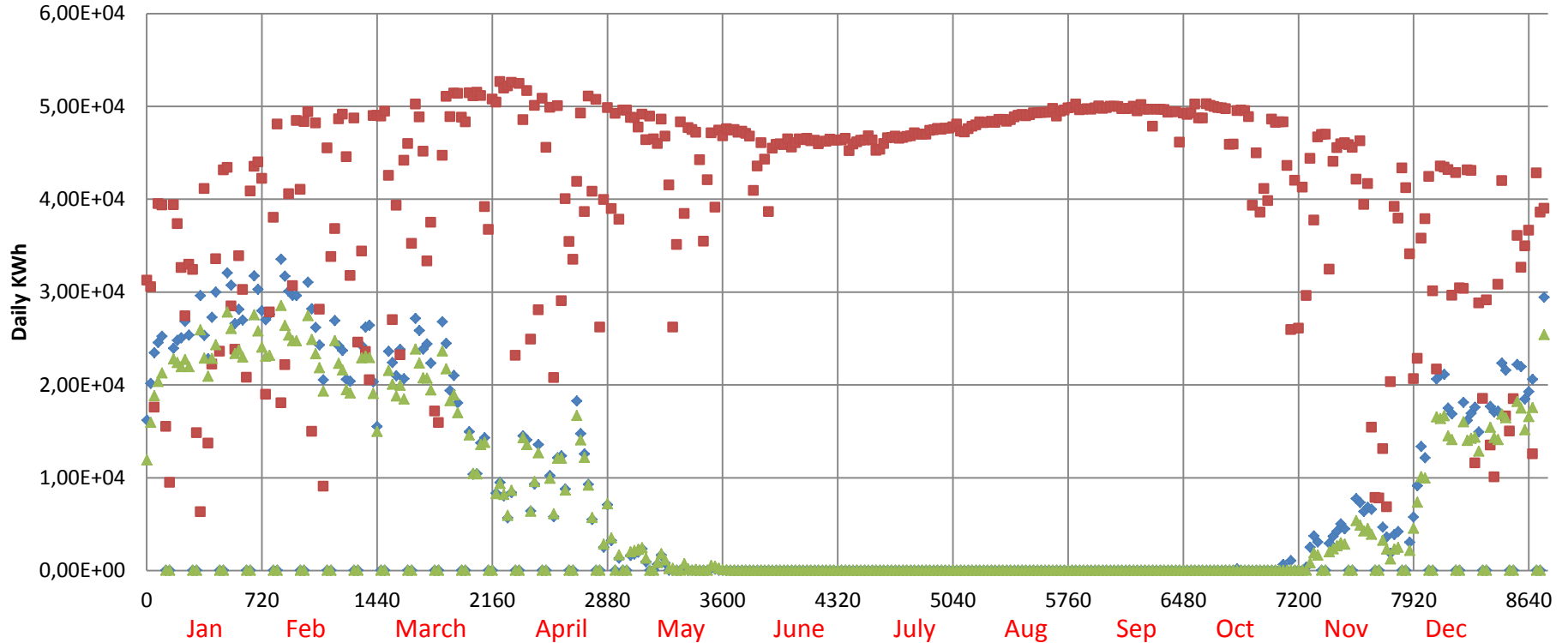
◆ Heating Demand wo ducts ■ Efficient Solar input/ 10m2 ▲ Heating Demand



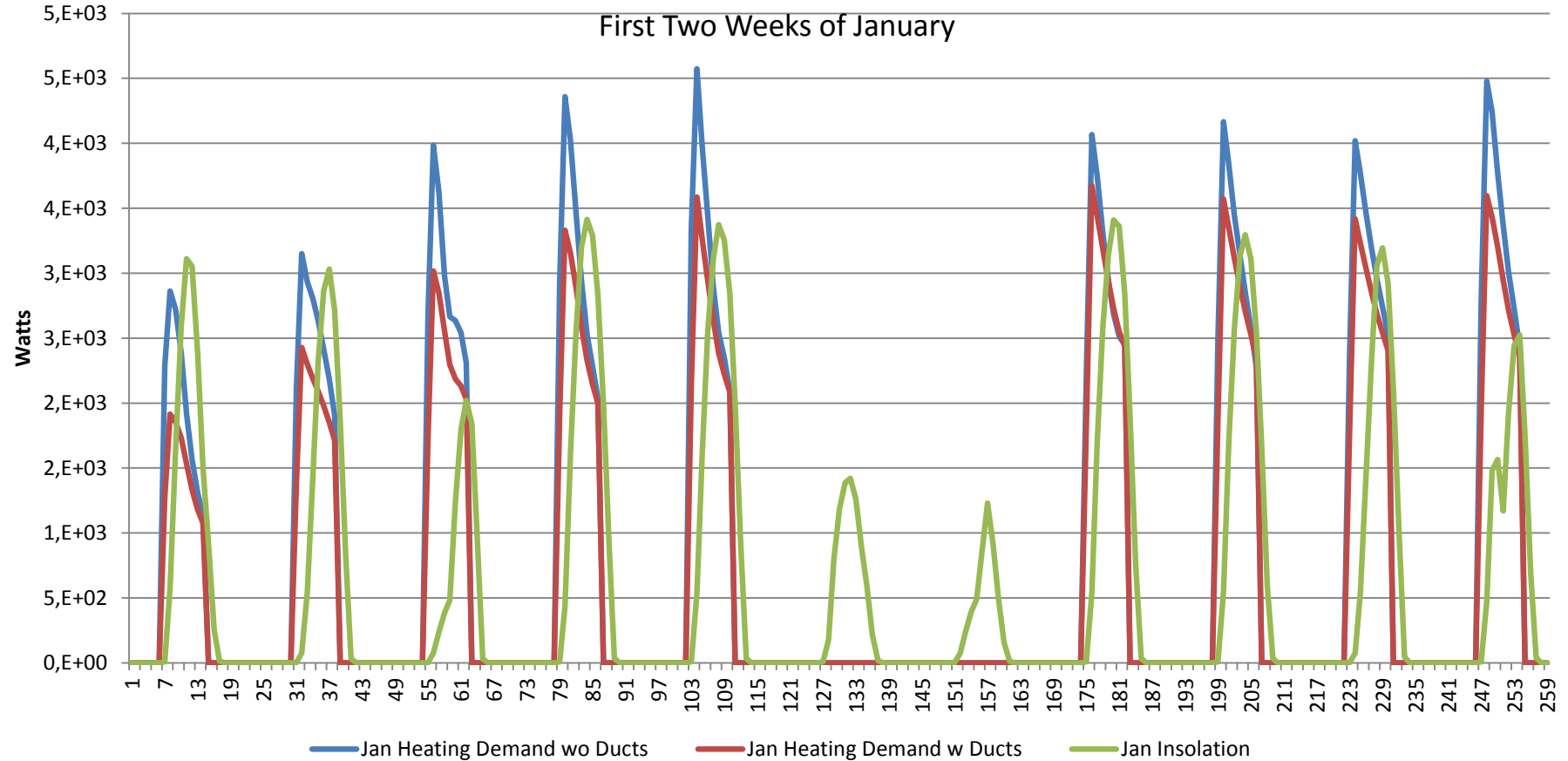
Solar Thermal - Primary Investigation

45° Tilted Surface Output vs Heating Demand

◆ Heating Demand wo ducts ■ Efficient Solar input/ 10m2 ▲ Heating Demand

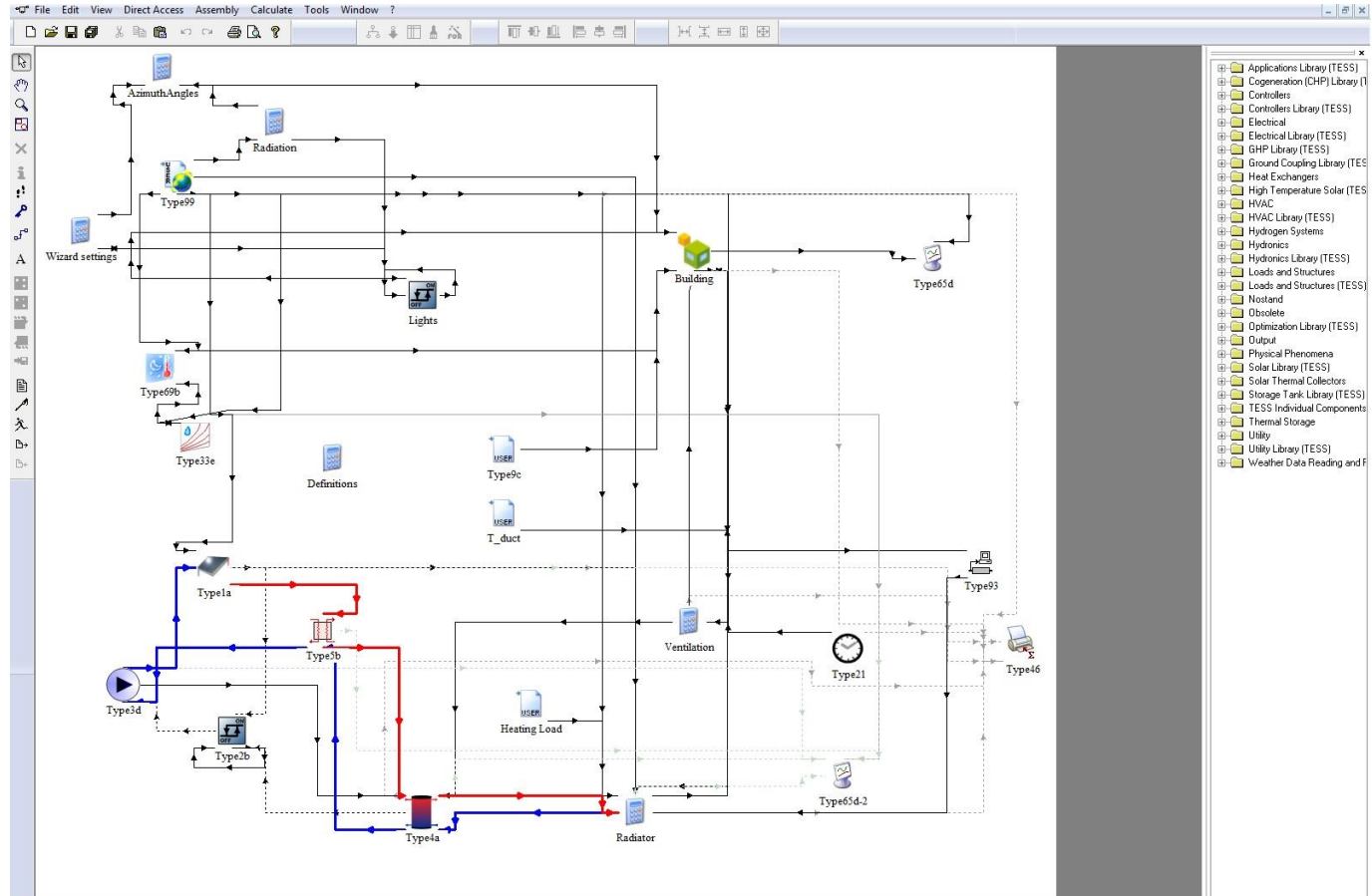


Solar Thermal - Primary Investigation

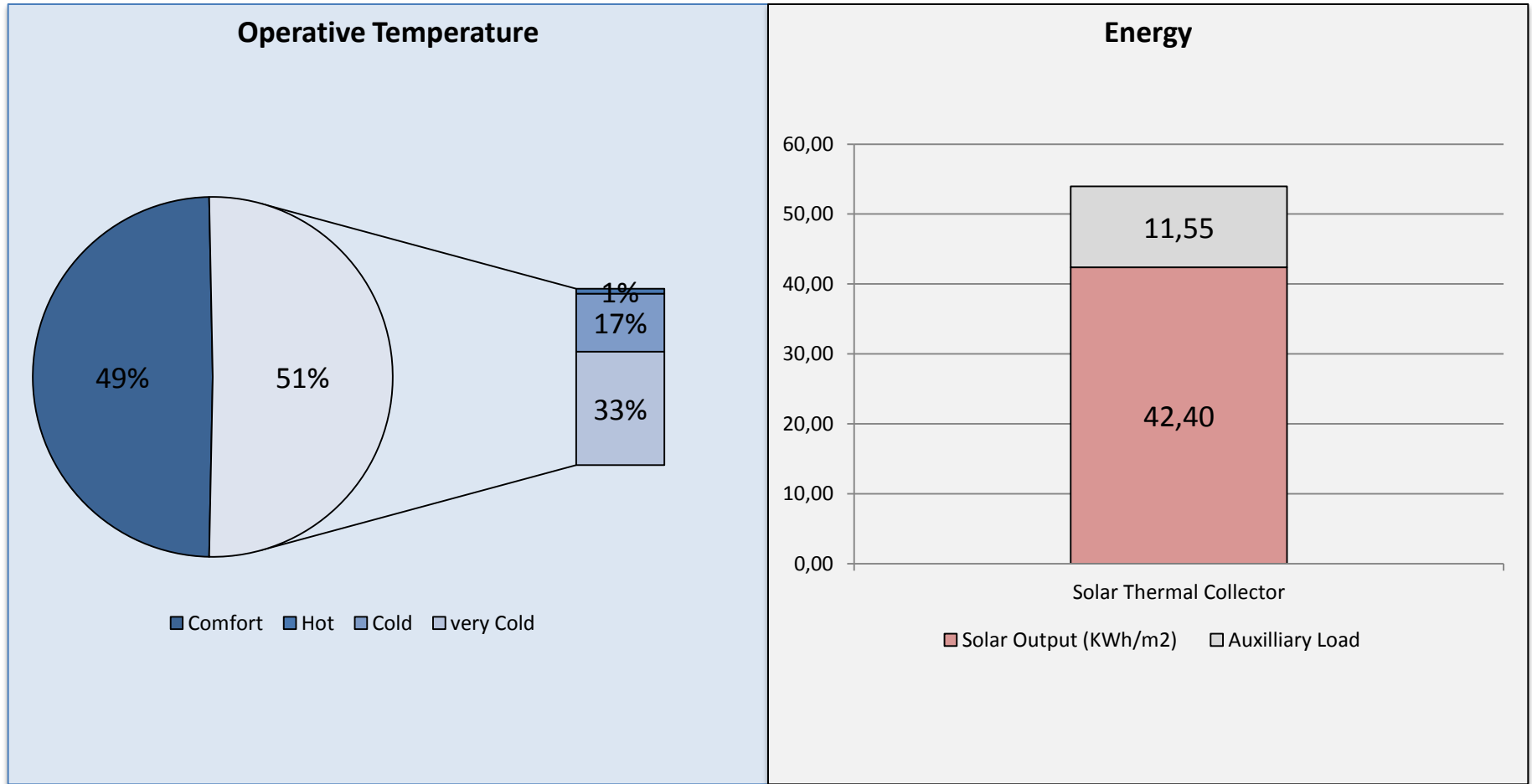


Solar Thermal

Snapshot- Trnsys Setup



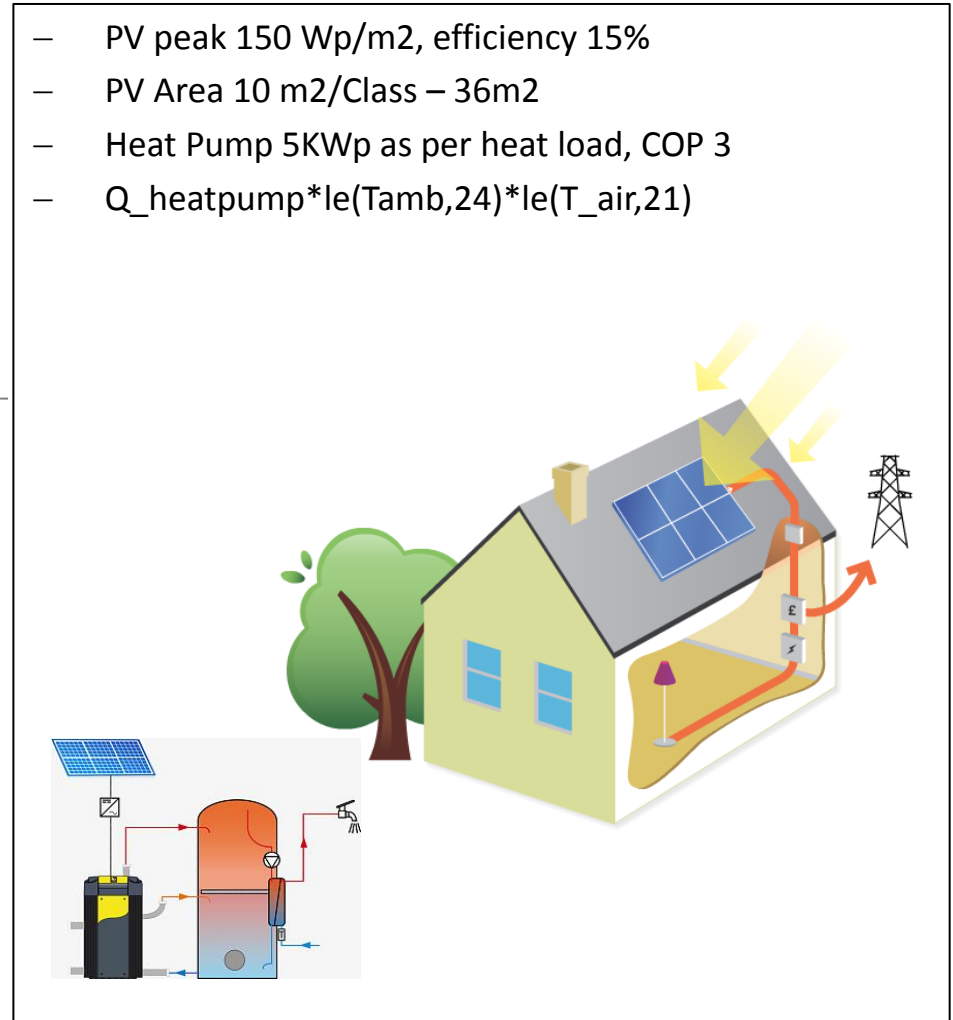
Solar Thermal Collector



Active Strategies

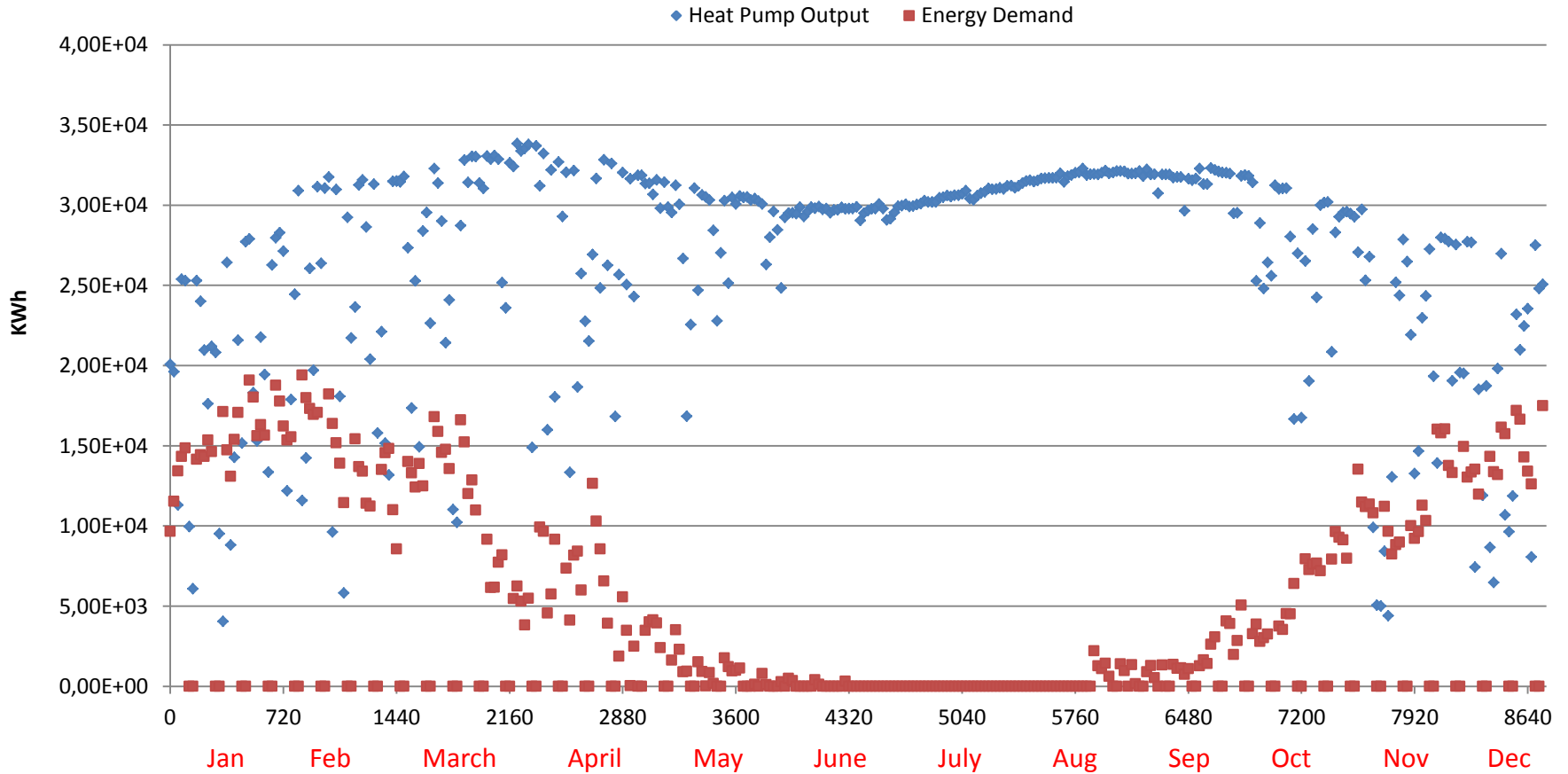
- Solar Thermal Collector
- PV + Heat pump
- AHU
- Solar Air Collector

- PV peak 150 Wp/m², efficiency 15%
- PV Area 10 m²/Class – 36m²
- Heat Pump 5KWp as per heat load, COP 3
- $Q_{\text{heatpump}} * \ln(T_{\text{amb},24}) * \ln(T_{\text{air},21})$

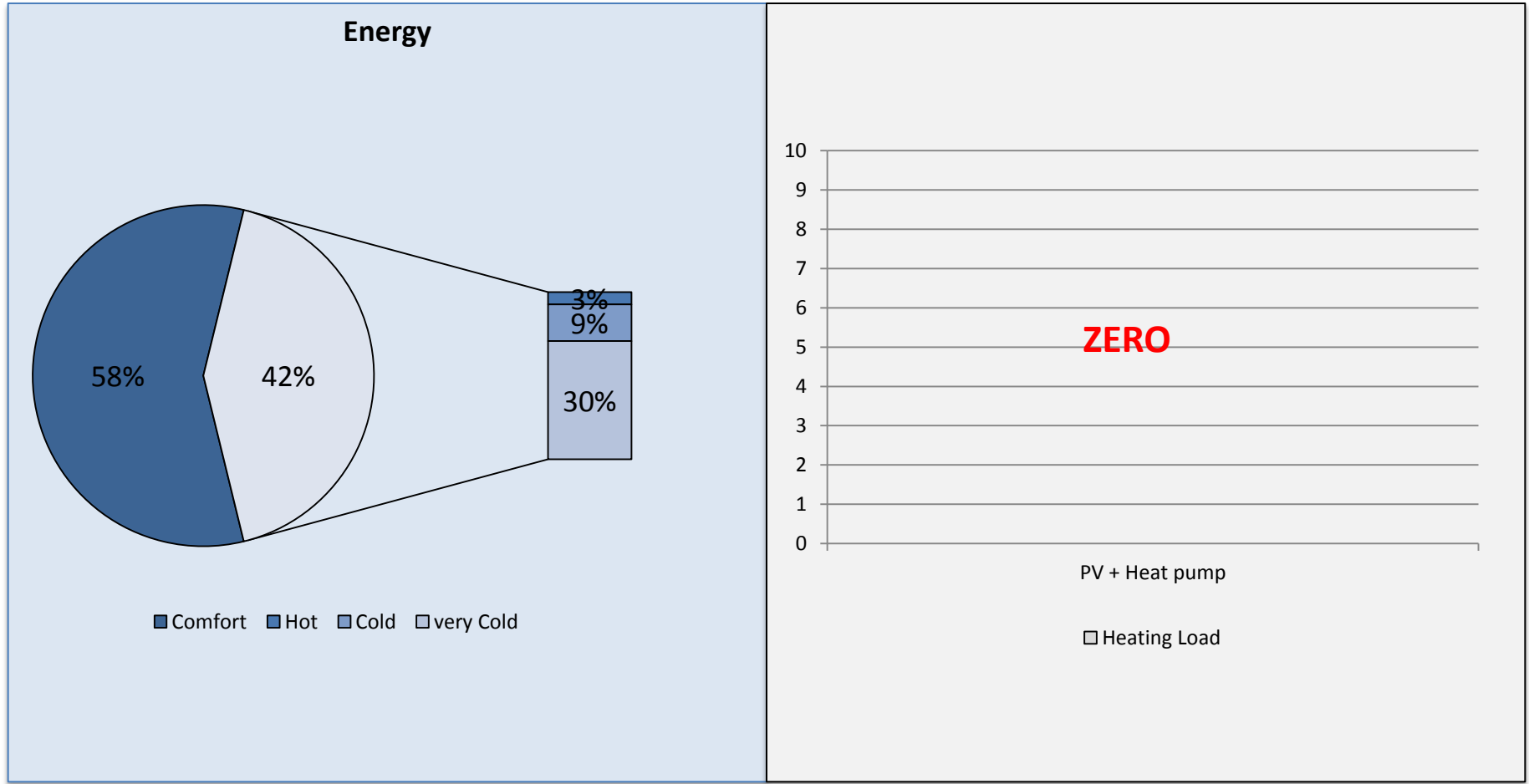


Primary Investigation

45° Tilted Surface Output vs Heating Demand



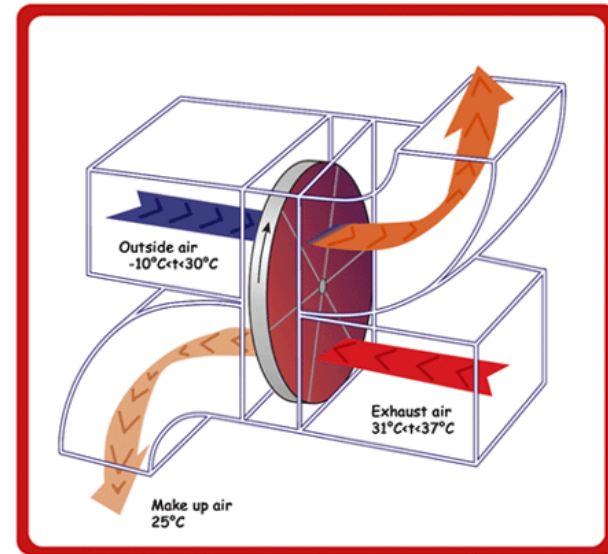
PV + Heat Pump



Active Strategies

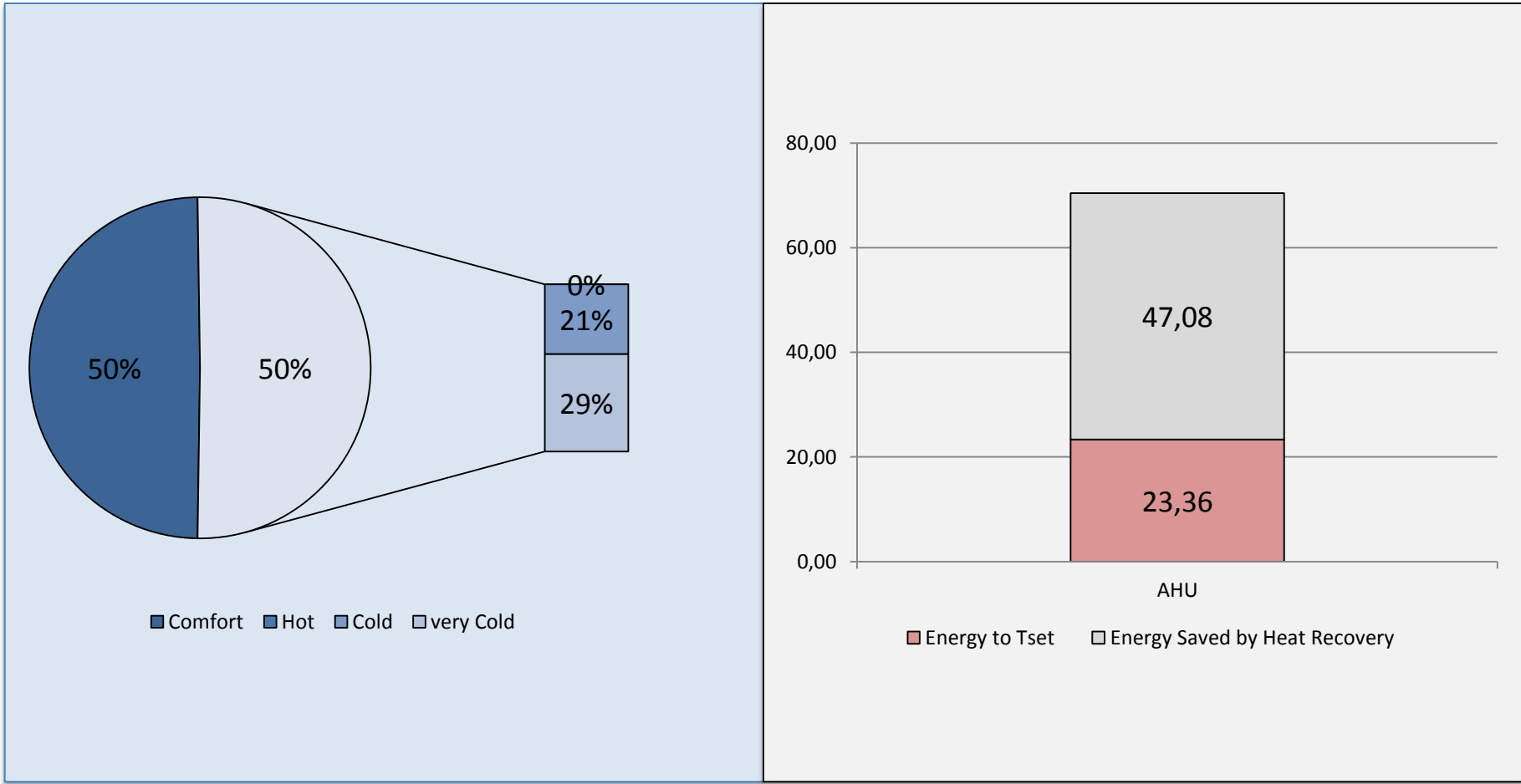
- Solar Thermal Collector
- PV + Heat pump
- AHU
- Solar Air Collector

- Set Temperature AHU= 21 for $T_{amb} < 21$
- Heat Recovery= 70% for $T_{amb} < 21$



A diagram of a rotary heat exchanger, or "heat wheel" (From Uptime Technology BV)

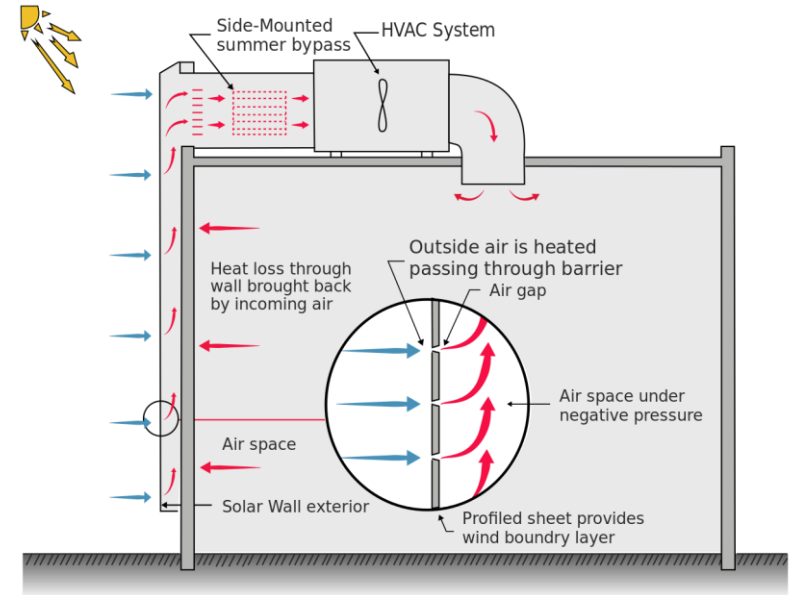
AHU



Active Strategies

- Solar Thermal Collector
- PV + Heat pump
- AHU
- Solar Air Collector

- Vertical Insolation south oriented
- Solar air heat source



Solar Air Collector

Primary Investigation

- Type 1 Glazed
- Efficiency 70%
- Vertical Setup – Directed to South
- $T_{out} = (((n \cdot G) / (C_p \cdot m_{flow})) + T_{amb}) \cdot \ln(T_{amb,24}) + \ln(T_{amb,24}) \cdot T_{amb}$

From these (and in accordance with equations IV.1.1 and IV.1.3) the following relations can be derived:

$$\dot{Q}_a = \eta G \quad (IV.1.4)$$

and

$$\Delta T = (T_o - T_i) = \frac{\dot{Q}_a}{\dot{m} C_p} = \frac{\eta G}{\dot{m} C_p} \quad (IV.1.5)$$

where A_c is chosen to be 1 for the normalized situation (per m²)

Flat-plate air collectors

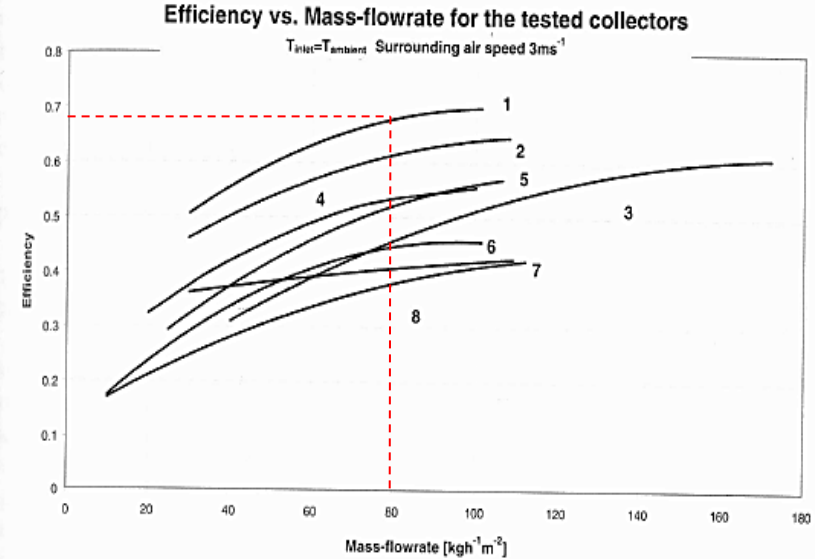
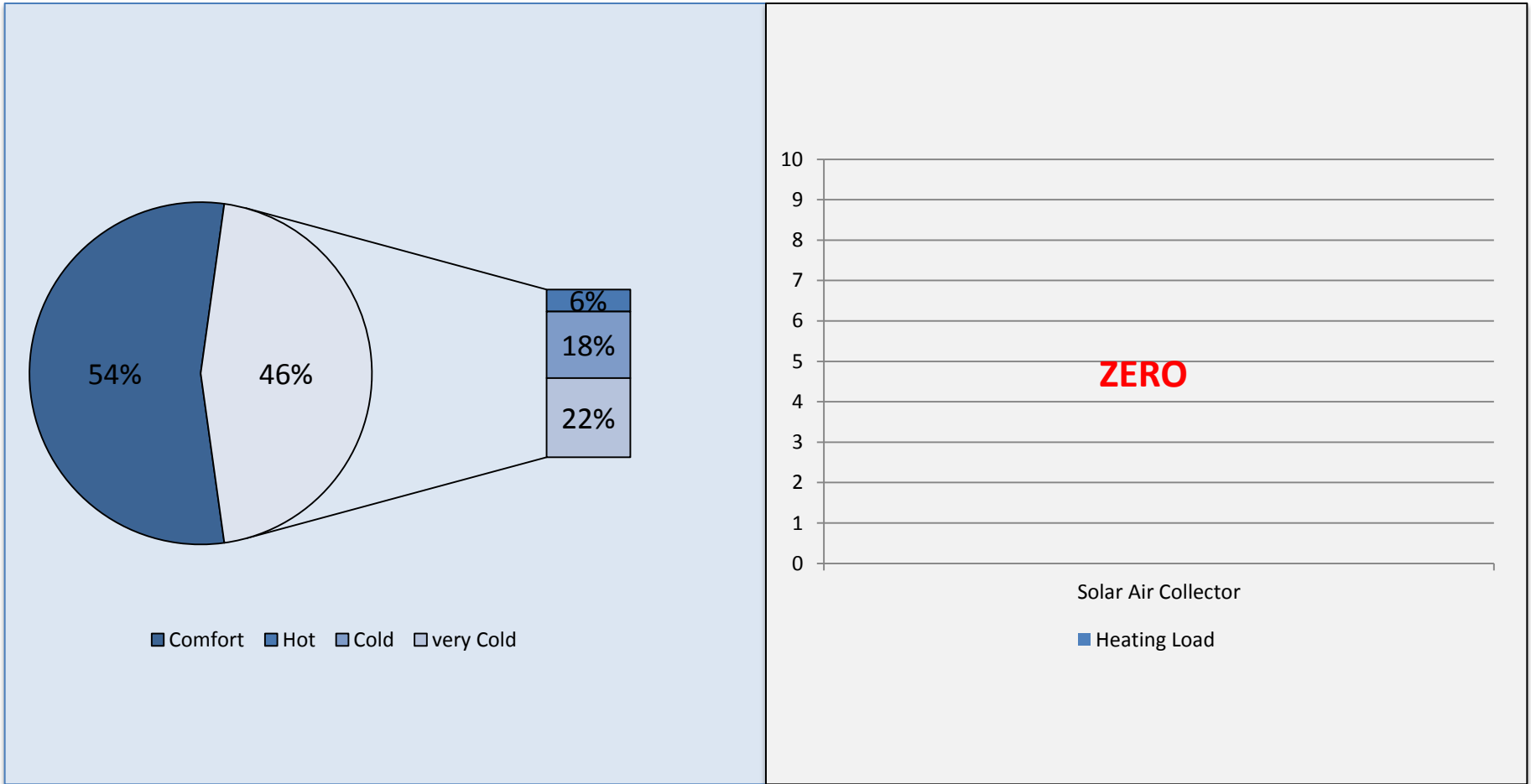


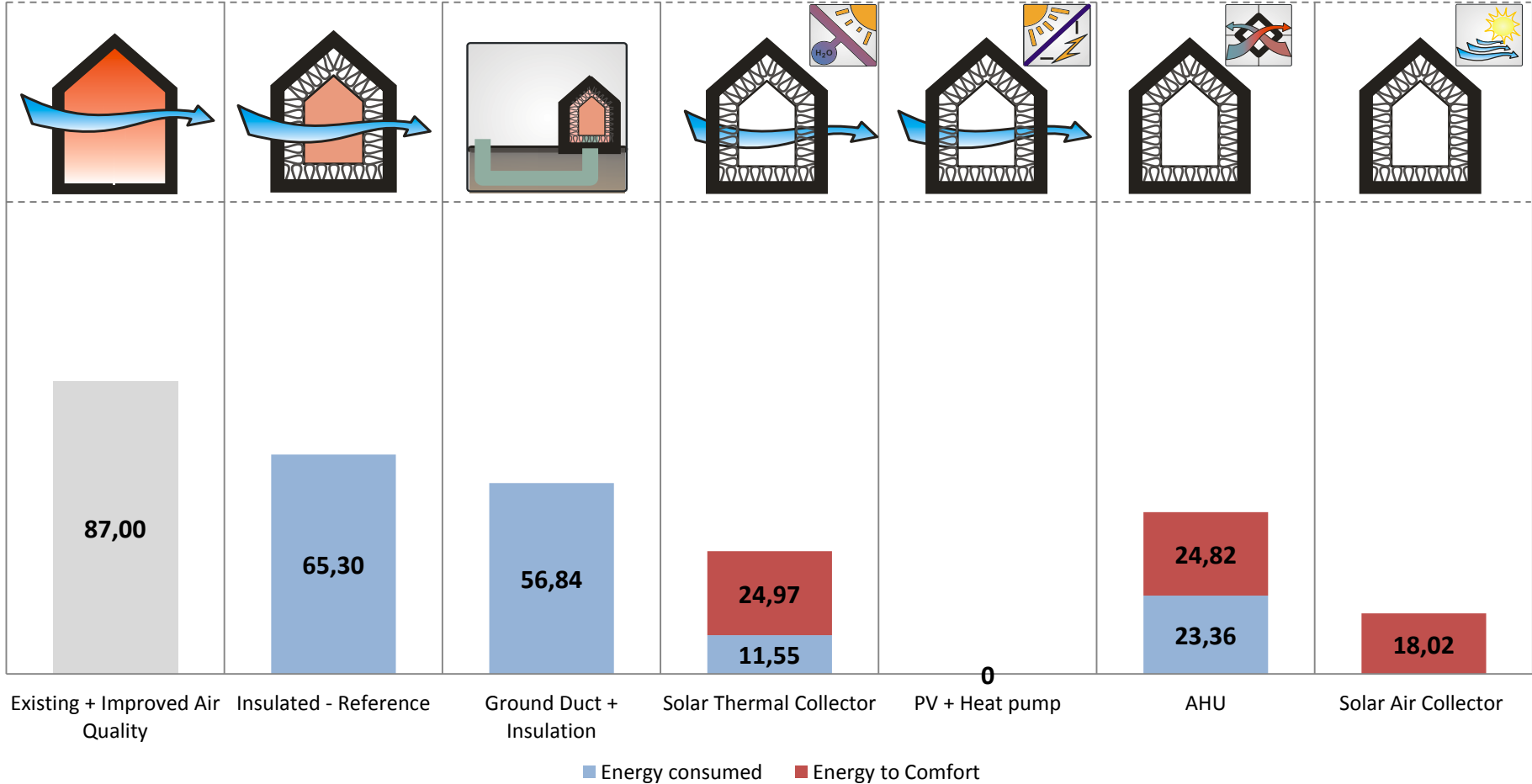
Figure IV.1.4. Efficiency versus mass-flow rate for selected collectors on the market

- 1 glazed collector (iron-poor), aluminum absorber with U-profiles, selective coating, underflow
- 2 glazed collector, black textile absorber
- 3 unglazed perforated trapezoid absorber panel, aluminum, anthracite, strongly dependent on wind (curve for 3 ms^{-1})
- 4 glazed plane absorber, black painted, facade element, underflow
- 5 glazed, rippled absorber, air flow on both sides
- 6 glazed plane absorber, black painted, facade element, air flow on both sides
- 7 glazed site-built collector, selective absorber, trapezoid profile, underflow
- 8 glazed plane absorber, black painted, facade element, underflow

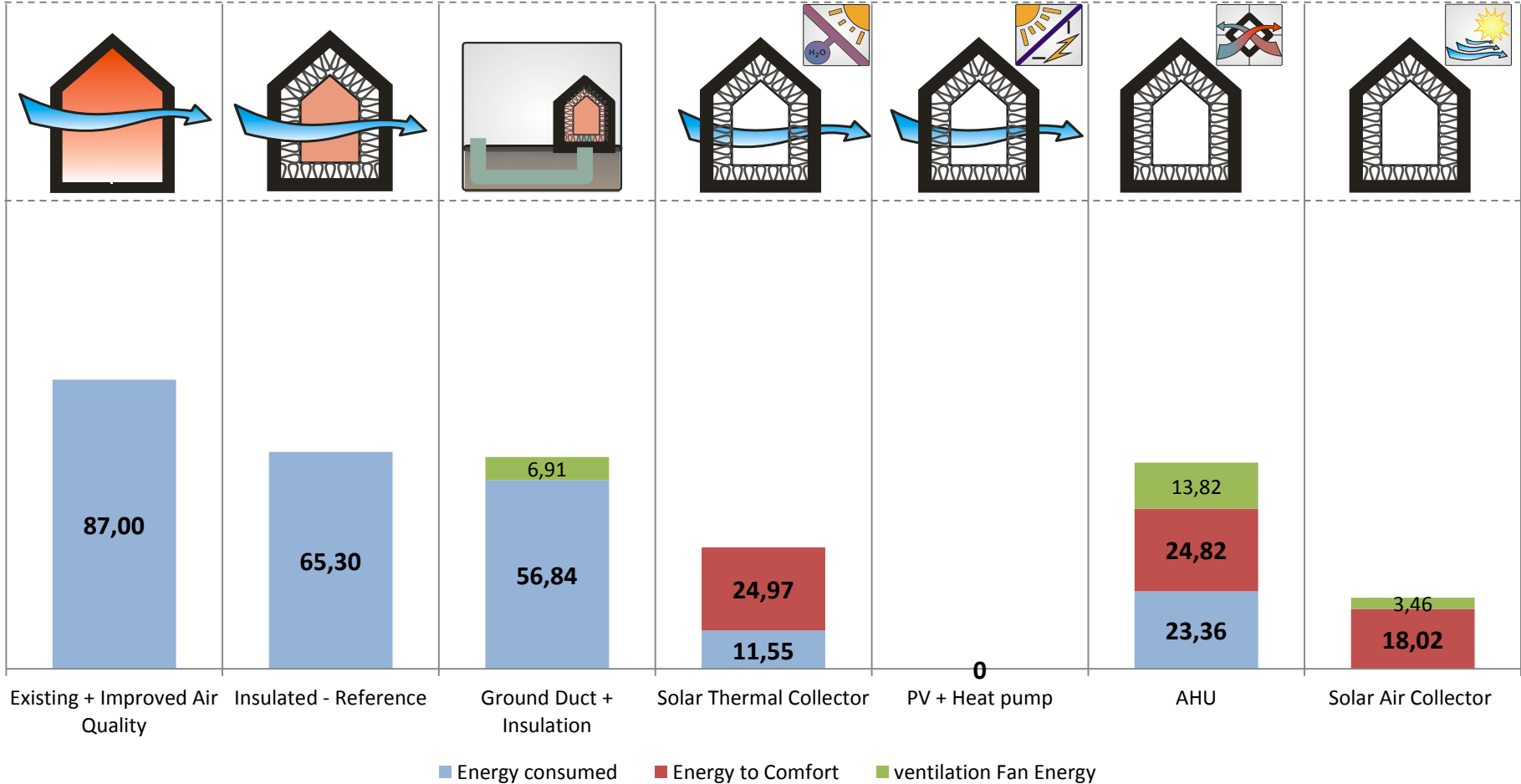
Solar Air Collector



Heating Load



Heating Load + Electric Fan Power



LCA and Cost Estimation

- Capital Investment
- Return Period

	Heating Load/m2	Energy Saved	Electric Required/m2	Cost of system/ unit	Ancillary Costs	Unit	Description
Existing (Trnsys)	55.75						
Existing + Improved Air Quality	87.00	0.00	0.00				
Insulated - Reference	65.30	21.70	0.00	10-13.5	5.00		Insulation + Plaster
Ground Duct	56.84	30.16	6.91	3298.67	9640.00	12 Classes - 432 m2	100 m duct/12 classes
Solar Thermal Collector	36.51	50.49	0.00	5666.67	1000.00	1 Class - 36 m2	10 m2 Panel-1 m3 tank/class
PV + Heat pump	0.00	87.00	0.00	2300.00	2500.00	1 Class - 36 m2	10 m2 PV + 5KWp Heat Pump
AHU	48.19	38.82	13.82	2160.00	0.00	12 Classes - 432 m2	4000 m3/h/ 12 classes
Solar Air Collector - Type 1	18.02	68.99	3.46	840.00	500.00	1 Class - 36 m2	5.6 m2 Type 1


	Effective Cost \$/m2	Total Costs	Total Cost \$/m2 (Bldg)	Cost of Energy Saved	Payback Time	Life Cycle	Feasibility
Insulated - Reference	\$30.13	\$54,243	\$19	\$4,395	10.23	30-40	Yes
Ground Duct	\$29	\$105,997.34	\$37.86	\$4,465	17.02	30-40	No
Solar Thermal Collector	\$185	\$387,575.98	\$138	\$10,224	23.53	15-20	No
PV + Heat pump	\$133	\$294,242.65	\$105	\$17,618	13.05	15-20	No
AHU	\$60	\$162,242.65	\$57.94	\$4,576	22.52	15-20	No
Solar Air Collector - Type 1	\$37	\$121,243	\$43	\$13,148	8.01	15-20	Yes

years	Insulated - Reference	Ground Duct	Solar Thermal Collector	PV + Heat pump	AHU	Solar Air Collector - Type 1
1	-\$47,931	-\$97,627	-\$362,838	-\$265,986	-\$151,603	-\$103,937
2	-\$41,862	-\$89,579	-\$339,052	-\$238,815	-\$141,373	-\$87,297
3	-\$36,026	-\$81,841	-\$316,181	-\$212,690	-\$131,536	-\$71,296
4	-\$30,415	-\$74,400	-\$294,189	-\$187,570	-\$122,077	-\$55,911
5	-\$25,020	-\$67,245	-\$273,044	-\$163,415	-\$112,982	-\$41,118
6	-\$19,832	-\$60,366	-\$252,711	-\$140,190	-\$104,237	-\$26,894
7	-\$14,844	-\$53,751	-\$233,161	-\$117,858	-\$95,829	-\$13,217
8	-\$10,047	-\$47,390	-\$214,362	-\$96,385	-\$87,743	-\$66
9	-\$5,435	-\$41,275	-\$196,287	-\$75,738	-\$79,969	\$12,579
10	-\$1,001	-\$35,394	-\$178,907	-\$55,885	-\$72,494	\$24,738
11	\$3,263	-\$29,740	-\$162,195	-\$36,795	-\$65,306	\$36,429
12	\$7,363	-\$24,303	-\$146,126	-\$18,440	-\$58,395	\$47,671
13	\$11,305	-\$19,075	-\$130,675	-\$791	-\$51,749	\$58,480
14	\$15,096	-\$14,048	-\$115,818	\$16,180	-\$45,359	\$68,874
15	\$18,741	-\$9,214	-\$101,533	\$32,497	-\$39,215	\$78,867
16	\$22,246	-\$4,567	-\$87,797	\$48,187	-\$33,307	\$88,477
17	\$25,615	-\$98	-\$74,589	\$63,274	-\$27,627	\$97,716
18	\$28,856	\$4,199	-\$61,890	\$77,781	-\$22,165	\$106,601
19	\$31,971	\$8,330	-\$49,678	\$91,729	-\$16,913	\$115,143



Recommendation and Future Steps

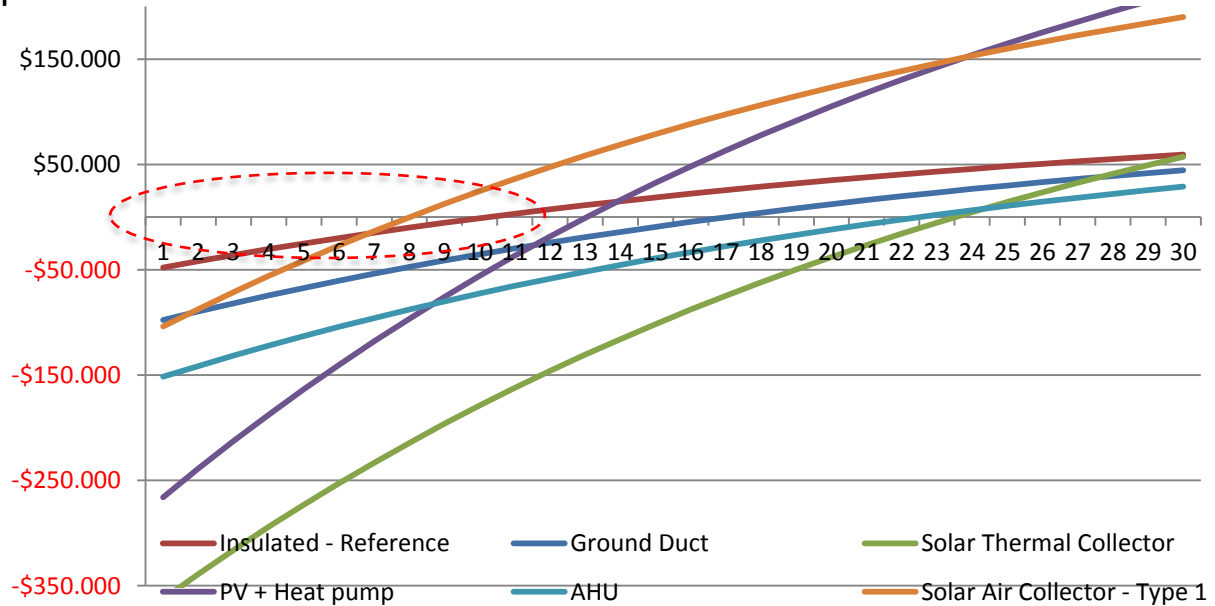
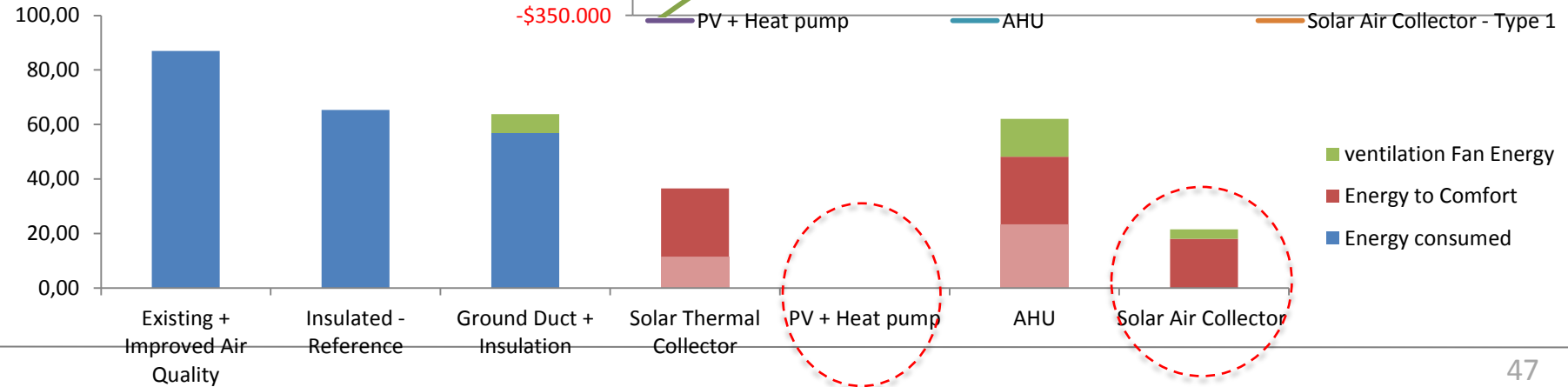
Which Investment is sexy?

Solar Air Collector 
 Total Cost + Insulation
 120,000 \$ or 92,000 euros

PV + Heat Pump
 295,000 \$ or 227,000 euros

Life Cycle

Technical System: 15-25 years
 Insulation: 30-40 years



Solar Air Collector



Solar Air Collector

Advantages

- No need to change the system
- Decentralized
- Aesthetic enhancement to the Facade (Simple system but looks fancy)
- Low Cost
- Easy to Implement
- Can be coupled with existing radiator system to meet comfort
- Low Maintenance
- Clean and Easy source of energy
- Less space needed with respect to other systems only 5.6 m²/ class

Future Steps

- Present the results to the school
- Hope that they are smart enough to adopt the recommended scheme



THANK YOU

TransSolar GmbH



Special Thanks

Peter Voit

Christian Degenhardt

Jochen Lam

Monika Schulz

Matthias Schuler

